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# PHASE 2 INTRUSIVE GROUND INVESTIGATION INTERPRETATIVE REPORT For 12 & 14 EDHILL AVENUE, SIMONSIDE, SOUTH SHIELDS NE34 9BJ

This report was carried out in accordance with JPB Quality Management procedures.

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#### 1.0 INTRODUCTION

- 1.1 Further to written instructions received on 18 November 2013 from South Tyneside Homes Limited (STH), Johnson Poole and Bloomer Limited (JPB) is pleased to present an Interpretative Ground Investigation Report for the site known as 12 & 14 Edhill Avenue, South Shields. The site's location and boundaries are shown on JPB Drawings NB503/01 and NB503/02, respectively.
- 1.2 This report has been written for STH and is required in order to determine the shallow and general ground conditions on site. This report also highlights any potential environmental risks and liabilities associated with the future redevelopment of the site, arising from its past and present uses. Information is provided relating to the on site ground conditions, together with any further issues which could lead to potential financial liabilities that may affect the land value or impact upon potential redevelopment options. At the time of writing, it is understood that STH is considering the redevelopment of the site for residential purposes.
- 1.3 JPB has previously prepared a Phase 1 Desk Study for STH at this site. That report is referenced NB503-12/ACJ/FT and dated 25 November 2013. Where relevant, information from this previous report has been utilised in conjunction with the information obtained from the current ground investigation.
- 1.4 As part of this commission, RP Drilling Limited was appointed by JPB as sub-contractor, to undertake windowless sample boreholes. The site works were undertaken on 9 January 2014 under the full time supervision of a JPB Geologist.
- 1.5 This report and its related documents have been prepared for the sole use of the specified client in response to an agreed brief, for a stated purpose and at a particular time and its application must be made accordingly. No duty of care extends to any other party who may make use of the information contained therein.
- 1.6 In reading this report, the information presented and discussed in Sections 9.0 and 10.0 (Conclusions and Recommendations and General) should be consulted and noted.



#### 2.0 SITE DESCRIPTION AND SETTING

### 2.1 Site Description

# General

2.1.1 The site comprises 12 and 14 Edhill Avenue, a pair of semi detached properties in the Simonside area of South Shields, approximately 2.5km to the southwest of Jarrow town centre. The centre of the site is at approximate National Grid Reference 435010, 564061, and the site's general location is shown on JPB Drawing NB503/01. Occupying an area of approximately 0.095ha, the site is rectangular shaped in plan view, with its longest axis orientated northeast to southwest. The site and its surroundings were generally level at an elevation of approximately 23m above ordnance datum (AOD). The site boundaries and layout are shown on JPB Drawing NB503/02.

#### **Site Boundaries**

2.1.2 The northern boundary was with the grounds of a large dwelling to the north and was marked by close timber board fencing and the site property itself. The westernmost edge of the northern boundary was not formally marked. The eastern and southern boundaries were also marked by close timber board fencing, with rear residential gardens beyond to the east and southwest. Two substation buildings were noted to the southeast. The western boundary was open and formed by the public footpath of Edhill Avenue, with residential properties beyond.

# **Adjacent Site Uses**

2.1.3 Edhill Avenue was located within a densely developed residential area, with various shops and schools in the vicinity.

#### Site Layout

- 2.1.4 The site comprised a pair of unoccupied semi detached dwellings, which were boarded up with metal plates at the time of the site inspection. The most recent use of the site was indicated by a plaque on the frontage of the building reading "Children and Young People Directorate, Leaving Care Services". The structure was a typical 1960's two storey red brick construction with a pitched tiled roof. A number of small extensions appeared to have been added to the building in the past and an external metal staircase to the first floor of the property was noted at the rear of the building.
- 2.1.5 In addition to the building, the site was occupied by soft landscaped areas, including a level grassed area to the site frontage and an overgrown garden to the rear. The soft landscaped areas were typically separated from the building by concrete slabs.
- 2.1.6 The rear garden was noted to predominantly comprise overgrown grass with areas of shrubs and brambles, typically towards the northeastern and eastern areas. There were no trees present on site. Discarded garden furniture was noted in the northwestern area of the garden whilst other discarded items (tent, clothing, timber, general rubbish etc) were generally present amongst the undergrowth throughout.



#### Site Access

2.1.7 The rear of the property could only be accessed via a narrow wooden (unsecured) gate at the southern boundary. The front of the site was freely accessible from the public footpath. As a result of the boarding, which appeared to remain intact, no access into the property itself was available.

#### 2.2 Site Setting

#### General

2.2.1 For full details of the site setting, reference should be made to the previous JPB Phase 1 Desk Study Report referenced NB503-12/ACJ/FT and dated 25 November 2013. A brief summary of the pertinent findings of the JPB desk study report is presented below.

#### History

2.2.2 Historically, the site was an undeveloped field until approximately 1957 when the historical plan shows the current structures as they appear today on site.

# Geology

2.2.3 Made Ground is anticipated across the site, and this is likely to comprise materials arising from the demolition and construction of roads and buildings both on and off site. The BGS published information indicates the site to be underlain by clay deposits of the superficial Pelaw Clay Member, with the Pennine Upper Coal Measures Formation (mudstones, siltstones, sandstones and coal) at depth.

#### Mining and Quarrying

- 2.2.4 The Non-Residential Coal Authority Mining Report indicates that the site is within the likely zone of influence on the surface from workings in 3 seams of coal at 380m to 460m depth, although any ground movement from these workings, last worked in 1955, should have now ceased. The site is not within the likely zone of influence on the surface from current or future underground coal workings and there are no recorded mine entries within, or within 20m of, the site boundaries. The report also indicates that the site is not located within the boundary of a former, current or proposed opencast site.
- 2.2.5 Information on the Coal Authority website indicates that the site is not located within a coal mining development high risk area and therefore a coal mining risk assessment report will not be required as part of the planning process.
- 2.2.6 Information from the BGS website indicates that there are no active quarries within a 1km radius of the site. In addition, consultation of the Department of the Environment (DOE) Review of Mining Instability in Great Britain (1991) indicates that there is inconclusive evidence of ground instability relating to coal mining within the area.
- 2.2.7 On the basis of the geological setting and information provided by the Coal Authority, GroundSure Report and that held within JPB's archives, mining is considered to be **not significant** to the site and its future redevelopment.



#### Hydrogeology and Hydrology

- 2.2.8 The Pelaw Clay deposits underlying the site are classified by the EA as Unproductive strata, whilst the Pennine Upper coal measures are Secondary A Aquifers. Groundwater is considered to be of low to moderate sensitivity and at a low risk from potential contamination on site.
- 2.2.9 There are no major surface water features within a 250m radius of the site. Based on the information reviewed, surface waters in proximity to the site are considered to be of negligible sensitivity and at low risk from potential contamination on site.

#### **Flooding**

2.2.10 The site is not located within a flood risk area for surface waters, fluvial flooding is therefore considered to be **not significant** to the site. There is also a negligible susceptibility to groundwater flooding on site; this is therefore considered to not be significant to the site.

#### Landfills and Waste Management Sites

2.2.11 There are no records relating to various waste management sites within 250m of the site. Waste management and treatment sites are considered to be **not significant** to the site and its future redevelopment.

#### Conceptual Site Model (CSM)

- 2.2.12 A CSM included in the JPB Phase 1 desk study report was derived on the basis of the findings of the same, Phase 1 Desk Study Ground Investigation Report, on the basis of a proposed residential end use. This model identified the sources, pathways and receptors from the existing information; and also identified the potential pollutant linkages for consideration in the investigation.
- 2.2.13 The JPB Phase 1 Desk Study Report concluded that there were limited source-pathway-receptor linkages on site, and that the site presented a low to moderate risk to the health of current and future site users and construction workers and a low risk to the environment, from potential chemical contamination on site. Further assessment by means of an intrusive ground investigation was recommended, in order to identify the actual pollutant linkages on site.
- 2.2.14 The risk from ground gases was considered to be **low** and is mainly attributable to the proximity of off site historic landfill sites. The risk to site users present from radon gas was considered to be **not significant**.
- 2.2.15 This report details the findings of the completed intrusive ground investigation.



#### 3.0 GROUND INVESTIGATION SCOPE OF WORKS

#### 3.1 Introduction

- 3.1.1 As previously stated, JPB was commissioned by South Tyneside Homes (STH) to undertake an intrusive ground investigation, with the proposed scope of works designed on the basis of the recommendations from the JPB Phase 1 Desk Study. This included investigations to establish the general shallow ground conditions, the contamination status and the groundwater and gas regimes on site. It is understood that information presented in this ground investigation report will be used to assist in determining the feasibility of the future redevelopment of the site.
- 3.1.2 The main objective of this investigation was to provide information sufficient for STH to determine the general ground conditions and identify any remediation or abnormal redevelopment issues associated with a potential future redevelopment of the site.
- 3.1.3 At the time of the ground investigation, preliminary development options had been proposed although detailed development plan had been determined. It is possible that further assessment may be required in the future, as the detailed design becomes available.

#### 3.2 Intrusive Investigation

- 3.2.1 The ground investigation fieldworks were undertaken by RP Drilling Ltd on 9 January 2014, under the full time direction and supervision of a JPB Geologist. The investigation was undertaken in accordance with BS5930:1999 (incorporating Amendment 2), with all exploratory holes logged in accordance with BSEN14688-1:2002 and BSEN1997-2:2007 by the supervising JPB Geologist.
- 3.2.2 The ground investigation comprised the following programme of works.
  - Five windowless sample boreholes, designated WS201 to WS205 advanced to a maximum depth of 7.45mbgl using a Global Geotech mini rig. In-situ geotechnical testing was carried out in the boreholes, comprising Standard Penetration Tests (SPT) where the number of blows required to drive a barrel sampler 300mm in to the base of the borehole is recorded as the 'N' value. Disturbed samples of the materials encountered were retrieved for both chemical and geotechnical laboratory testing. All in-situ test results and sample details are recorded on the individual exploratory hole records presented in Appendix B.
  - Standpipes for monitoring gas and groundwater, and also to undertake preliminary infiltration testing, were installed under the instruction of the JPB Geologist in three of the windowless sample boreholes. Details of the installations are shown on the individual exploratory hole records presented in Appendix B.



- Preliminary infiltration testing was undertaken during the subsequent monitoring period, in all of the installed boreholes on site.
- 3.2.3 The positions of the various exploratory holes are shown on JPB Drawing NB503/14.

# 3.3 Gas and Groundwater Monitoring

- 3.3.1 Upon completion of the ground investigation site works, a programme of ground gas and groundwater monitoring was undertaken in order to ascertain the on site gas and groundwater regimes. These installations, WS202, WS204 and WS205, were monitored on six separate occasions.
- 3.3.2 During each monitoring visit, the concentrations of methane, carbon dioxide, oxygen, hydrogen sulphide and carbon monoxide were recorded, together with atmospheric pressure, borehole pressure and gas flow at each installed position. A GA5000 infra red gas analyser was utilised to obtain these readings.
- 3.3.3 The gas monitoring is discussed in Section 7.0 of this report and the full gas monitoring results are presented in Appendix D.
- 3.3.4 The level of any groundwater encountered in the monitoring wells was recorded on each visit, in order to identify and characterise any underlying groundwater regime.
- 3.3.5 The water monitoring results are discussed in Section 4.0 of this report and the full monitoring results are presented in Appendix D.

# 3.4 Chemical Laboratory Testing

- 3.4.1 Soil samples were obtained from the exploratory positions at varying depths within the soil profile. Samples were selected on the basis of specific on site observations, the strata encountered, specific historic land use and the proposed redevelopment. All samples were analysed for a range of parameters to provide an indication of the overall nature, extent and severity of contamination present on site and to enable the appropriate risk assessment to be undertaken.
- 3.4.2 Soils from the exploratory holes were sampled by the supervising JPB Geologist and dispatched to Chemtest, a UKAS and ISO 17025 accredited laboratory that participates in the MCERTS scheme. The samples were transported in the supplied proprietary containers, under chilled conditions. The chemical analyses were scheduled by an experienced JPB Geologist for a broad suite of determinands, specified with reference to the site's former and current use and observations made on site. The chemical laboratory analytical results are presented in Appendix E of this report.
- 3.4.3 In total, five soil samples obtained from the boreholes were scheduled and analysed for some, or all, of the following determinands;



- Inorganic elements and compounds arsenic, barium, beryllium, boron, cadmium, chromium, hexavalent chromium, copper, lead, mercury, nickel, selenium, zinc, vanadium, sulphate (water soluble), free and total cyanide, pH and asbestos screening;
- Organic compounds USEPA 16 speciated polycyclic aromatic hydrocarbons (PAH), total petroleum hydrocarbons with aliphatic and aromatic split and carbon banding in accordance with the Criteria Working Group (CWG), including MTBE and BTEX, total phenol, total organic carbon (TOC) and the ICES 7 and WHO 12 polychlorinated biphenyls (PCBs) congeners.
- 3.4.4 First groundwater samples were obtained and tested for a similar suite of analysis as the soils with the addition of total alkalinity, electrical conductivity and sulphide. Groundwater samples were obtained from WS202 during the first monitoring visit, which was completed approximately two weeks following the installation of the boreholes, to allow ground conditions to equilibrate.

#### 3.5 Geotechnical Laboratory Testing

- 3.5.1 On the basis of observations made in the field, selected disturbed and undisturbed soil samples were scheduled by JPB for geotechnical laboratory analysis. The analysis was undertaken by GEO Site & Testing Services Limited at their UKAS accredited laboratory and was carried out in accordance with BS1377:1990. The following tests were conducted:
  - 3 No. Moisture Content;
  - 3 No. Atterberg Limits (plastic limit, liquid limit, plasticity index);
- 3.5.2 The geotechnical laboratory test results are presented in Appendix C.



#### 4.0 GROUND CONDITIONS

#### 4.1 General

- 4.1.1 Ground conditions encountered during the ground investigation works were generally consistent with the published BGS information. A brief description of the materials encountered on site is included in the following sections.
- 4.1.2 The generalised geological sequence beneath the site determined from the ground investigation is summarised in Table 4.1 below.

**Table 4.1: Generalised Geological Sequence** 

STRATA ENCOUNTERED AND DESCRIPTION	RANGE OF THICKNESS (m)	DEPTH TO BASE (mbgl)			
A. MADE GROUND					
A1 Soft dark brown slightly gravelly clay or silt.	0.30 - 0.50	0.30 - 0.50			
B. NATURAL SUPERFICIAL					
B1 Firm to stiff light brown mottled light grey slightly gravelly clay.  Pelaw Clay Member	0.55 – 1.80	1.00 - 2.30			
B2 Stiff chocolate brown gravelly clay. Occasional cobbles. Pelaw Clay Member	Not fully penetrated	Not fully penetrated			

#### 4.2 Made Ground

- 4.2.1 Made Ground Materials were encountered in each of the exploratory positions across the site. The average thickness of Made Ground deposits across the site was generally between 0.30m and 0.50m with the greatest total thickness of 0.50m encountered in WS205. The minimum thickness of 0.30m was encountered in WS203.
- 4.2.2 The Made Ground materials were generally consistent across comprising predominantly re-worked natural materials as well as man-made materials such as demolition rubble.
- 4.2.3 For a full description of the Made Ground, reference should be made to the individual exploratory hole logs presented in Appendix B.

# 4.3 Natural Superficial Deposits

4.3.1 Natural superficial deposits were encountered in all exploratory positions beneath the identified Made Ground materials. The majority of the materials identified during the course of the ground investigation were determined to represent Pelaw Clay materials. The Pelaw Clay typically comprised slightly gravelly to gravelly clay with the gravel consisting of coal, sandstone, quartzite and mudstone. Cobbles of quartzite and sandstone were also present from below 3.0m.



- 4.3.2 The material was typically identified to be predominantly cohesive with a varying granular component comprising fine and medium gravel, with coarse gravels and cobbles below 3.0m bgl. The materials encountered are consistent with a typical Pelaw Clay deposit.
- 4.3.3 For a full description of the materials encountered within the natural superficial deposits, reference should be made to the individual exploratory logs presented in Appendix B.

#### 4.4 Groundwater

- 4.4.1 Groundwater was encountered during the intrusive site works within WS201, WS202 and WS203 as they were advanced, at a depth of between 0.60m and 0.80m bgl within the upper sections of the Pelaw clay. None of the other exploratory holes encountered groundwater during the course of the intrusive works on site.
- 4.4.2 Exploratory holes WS202, WS204 and WS205 were fitted with standpipe installations, predominantly to allow for gas monitoring and also for groundwater monitoring. The response zones, standpipe depths and levels of groundwater encountered are shown on the exploratory hole records in Appendix B.
- 4.4.3 The groundwater encountered during the monitoring period is considered to represent shallow perched water bodies within the Natural Superficial deposits. The perched water is likely to occur as discontinuous bodies within rare granular lenses within the superficial clays.
- 4.4.4 The resting groundwater levels recorded during the monitoring period are noted to have risen significantly when compared to the depths groundwater was encountered at during drilling. It is considered that this rise in groundwater may be indicative of sub-artesian pressures on the groundwater having been released by the penetration of the overlying materials.
- 4.4.5 The full groundwater monitoring results are presented in Appendix D.



#### 5.0 ENGINEERING PROPERTIES OF MATERIALS ENCOUNTERED

# 5.1 Engineering Properties

- 5.1.1 For the purposes of determining the engineering properties of the encountered materials, reference has been made to both in-situ and laboratory geotechnical testing.
- 5.1.2 The results of the in-situ and laboratory geotechnical testing of the samples recovered during the recent investigation are presented in Appendix C. The soil parameters from the in-situ and laboratory testing of samples are summarised in the following sections. It should be noted that the results may not be representative of the deposits as a whole due to the variation in both material types and depositional state across the site.

#### 5.2 Made Ground

- 5.2.1 Made Ground deposits were identified at all of the exploratory hole positions across the site and proved to be variable in their strength, thickness and composition. Aside from the obvious man-made materials that appeared to be derived from demolition waste (brick, concrete etc) the majority of materials comprised reworked natural materials.
- 5.2.2 Given the limited extend of the Made Ground deposits it was not considered necessary to undertake any specific geotechnical testing on these materials.

# 5.3 Pelaw Clay

5.3.1 Materials considered to represent the Pelaw Clay were encountered in all exploratory holes across the site below the identified Made Ground deposits. The Pelaw Clay was noted to be slightly variable in composition with a variable granular content.

**Table 5.1: Testing Summary Table for Pelaw Clay** 

Parameter	No. of Tests	Minimum	Maximum	Typical Result
Moisture Content (%)	3	15.5	33.8	Variable
Liquid Limit (%)	3	37	48	37-48*
Plastic Limit (%)	3	16	24	16-24*
Plasticity Index (%)	3	17	24	17-24*
Modified Plasticity Index (%)	3	15	19.5	15-19.5*
Soil type based on plasticity chart	3	Intermediate	Intermediate	Intermediate
Volume Change Potential	3	Low	Low**	Low**

<sup>\*</sup> Variable with material type, see text.

5.3.2 Atterberg limits testing identified that the Pelaw Clay materials were of intermediate plasticity with plasticity indices of between 17 and 24. Using the modified plasticity indices it was determined that the Pelaw Clay materials would be classified as a low volume change potential material under the NHBC guidance.

<sup>\*\*</sup> Assumes Modified Plasticity Indices are used for the determination.



- 5.3.3 Limited in-situ testing with a hand held shear vane recorded undrained shear strength values for the Pelaw Clay of between 45kN/m² and in excess of 120kN/m² with 'typical' values of between 60kN/m² and 70kN/m² recorded.
- 5.3.4 Limited in-situ testing using the SPT gave N values between and 25, with the majority of results between 11 and 34 with typical results varying between 13 and 17. There was no consistent variation in N value with depth across the site while the variation noted in the N values could partly be explained by the variation in granular content of the Pelaw Clay materials. Based upon the test results it is considered appropriate to assign an N value of 14 between 1.0m bgl and 2.0m bgl. It is possible to derive undrained shear strengths from SPT N values with typical results in the order of 55kN/m² to 75kN/m².
- 5.3.5 Based upon the testing, it is suggested that 55kNm<sup>-2</sup> be adopted as a suitably conservative value for undrained shear strength for further design purposes.

# 5.4 Summary of Characteristic Geotechnical Parameters

5.4.1 Table 5.2 contains a summary of the characteristic geotechnical parameters for the various strata identified during the current ground investigation. Given the noted variation of the deposits across the site it is considered that any future structures should be designed on an individual basis using the exploratory holes closest to the proposed structure, rather than using 'site wide' parameters.

# **Table 5.2 Summary of Characteristic Geotechnical Parameters**

	Ctrotum	Bulk		Undrained		Sulphate Class		Remarks
Stratum	Stratum Code	Density	Plasticity	Shear Strength	N Values	DS	AC	
	Code	(Mg/m <sup>3</sup> )		c <sub>u</sub> (kNm <sup>-2</sup> )		Class	Class	
Made Ground	A1	19.0	Intermediate	N/A	see note 2	N/A	N/A	
Dolow Clov	B1	19.0	Intermediate	55	12-13	DS-1	AC-1s	
Pelaw Clay	B2	19.0	Intermediate	65	14-17	DS-1	AC-1s	

#### Notes:-

<sup>1)</sup> The recommended parameters shown above are indicative for the whole site. Local variations in soil and rock properties will occur across the site. Structure / location specific checks should be undertaken to determine appropriate geotechnical parameters prior to detailed design.

2) Given the high variability in composition of the Made Ground deposits it is not considered appropriate to provide characteristic geotechnical parameters. Location specific checks will be

necessary.



#### 6.0 GEOTECHNICAL AND FOUNDATION CONSIDERATIONS

#### 6.1 General

- 6.1.1 At the time of writing, it is understood that STH is considering the redevelopment of the site for residential purposes. No indicative development layout or any indicative structural loads have been supplied to JPB although it is understood that traditional residential structures are planned.
- 6.1.2 Based upon the engineering properties of the shallow soils discussed in Section 5.0, the following preliminary comments are offered regarding suitable founding horizons. All depths quoted are relative to the site levels at the time of investigation.
- 6.1.3 The following foundation recommendations are considered to be for general guidance only and further professional geotechnical advice should be sought once the building loads and the final development proposals, including levels, are known. Depending upon the nature of the final development and of any proposed earthworks operations, further ground investigation may be required to allow detailed foundation design.

# 6.2 General Guidance for Foundation Design

- 6.2.1 The shallow Made Ground deposits were noted to be highly variable in terms of thickness, composition and strength across the site and are not generally considered appropriate for use as a founding medium.
- 6.2.2 The underlying Pelaw Clay derived cohesive strata are broadly considered acceptable for founding purposes. The Pelaw Clay materials would be classified as 'low' volume change potential materials under the NHBC guidance using their 'modified' plasticity indices. As such, a minimum founding depth of 1.0m bgl will be applicable assuming restricted new planting or the presence of existing trees or vegetation within influencing distance of the future foundations. Outside the zone of influence of any proposed or existing trees or vegetation the minimum founding depth will be 0.75m bgl provided that a suitable foundation stratum exists at this level. It will be necessary to check the formation level for suitability on a per plot basis, to ensure that minimum undrained shear strength of 55kNm<sup>-2</sup> is available. This should be done using a hand held shear vane with a minimum sample size of eight to ten tests per plot, spaced out across the whole building footprint.
- 6.2.3 Assuming a founding depth of 1.0m bgl a maximum net allowable bearing pressure of 80kNm<sup>-2</sup> is considered appropriate for future foundations, so as to limit settlement to less than 25mm. Conventional strip footings are considered appropriate for use for up to two storey traditional brick built structures. Should higher bearing pressures be required then it may be necessary to adopt semi-raft style foundations so as to spread the imposed structural loads over a larger area.



# 6.3 Concrete Design

- 6.3.1 For the purpose of designing sub-surface concrete to BS EN 206-1/BS50, guidance has been obtained from BRE SD1:2005 "Concrete in Aggressive Ground". The site has been classified as 'brownfield with "static groundwater" based upon the guidance documentation.
- 6.3.2 Determination of the water soluble sulphate content of near surface and deep soils was undertaken from four soil samples from across the site. The highest water soluble sulphate concentration was 20mg/l whilst the pH values across the site were found to vary between 7.3 and 8.3. A sample of groundwater recovered during the monitoring programme recorded a sulphate level of 120mg/l in WS202.
- 6.3.3 The data set used for the concrete classification assessment comprised fourteen soil samples, and following the guidance contained within BRE SD1:2005, the highest sulphate result was taken as the characteristic value. The soil characteristic value has therefore been calculated as 100mg/l (rounded up) whilst the water characteristic value has been rounded up to 200mg/l. These results place the site within Design Sulphate Class DS-1 and ACEC class AC-1s as derived from Table C2 in BRE SD1:2005 for 'static' groundwater. This corresponds to a Design Chemical Class (DC) of DC-1, assuming a designed working life of 100 years.

# 6.4 Drainage and Infiltration

- 6.4.1 As referred to in Section 3.0, preliminary infiltration testing was undertaken in the installed boreholes on site. Based on the results of the preliminary testing undertaken, the encountered geology at this site is **not considered suitable** for the use of infiltration style drainage for the collection and disposal of run-off waters as a result of the identified presence of effectively impermeable clay strata across the majority of the site.
- 6.4.2 As such, it is considered that attenuation storage may need to be provided to allow any future construction to meet its obligations under PPS25. Attenuation storage could take the form of lightweight honeycombed tanks beneath areas of hard standing / car parking and would require further assessment at the design stage.
- 6.4.3 Careful design and diligent supervision of the installation of any attenuation storage would be required, as any leakage could cause shrinkage / heave problems within the identified shrinkable soils on the site. JPB would be pleased to assist by preparing a Flood Risk Assessment for the site, if so required.



# 6.5 Services

6.5.1 All services **should** be designed to be flexible and be able to accommodate potential movements of up to 50mm. Excavated trenches to depths of approximately 1.2m should be relatively stable for short durations (i.e. hours) but may need to be battered to 1v in 0.6h should they need to be kept open for longer periods. Trenches deeper than 1.2m should be shored for safety and no man entry allowed under any circumstances.

#### 6.6 General Comments

6.6.1 During site works, should any localised softening of the soils be encountered then these materials should be removed and replaced with well compacted hardcore. In addition, it is imperative that the foundation excavations are kept dry to ensure the integrity of the cohesive deposits, as this material is potentially sensitive to wetting. All excavations should be examined to ensure that the formation level material is consistent with that used in this assessment.

#### 7.0 GROUND GAS EMISSIONS

# 7.1 General

- 7.1.1 During the intrusive investigation, monitoring instrumentation was installed in 3 of the windowless sample boreholes, namely WS202, WS204 and WS205.
- 7.1.2 The assessment of ground gas as a potential constraint to development has been the subject of considerable research and published guidance. Ground gas can be a concern for several reasons; flammable gases may cause an explosion, build up of gases within poorly ventilated areas may lead to asphyxia, and toxic gases may cause harm to those exposed to them. Some physical properties of ground gases are tabulated below.

**Table 7.1: Physical Properties of Ground Gases** 

Gas	Explosive Range	Density at 20°C	Toxicity (% by volume in air)*	
Methane (CH <sub>4</sub> )	5-15% by volume	0.72 kg/m <sup>3</sup>	30 (low)	
Carbon dioxide (CO <sub>2</sub> )	N/A	1.98kg/m <sup>3</sup>	0.5 (high)	
Carbon monoxide (CO)	10.5-74.2% by volume	1.25kg/m <sup>3</sup>	0.02 (high)	
Hydrogen sulphide (H <sub>2</sub> S)	rogen sulphide (H <sub>2</sub> S) 4.2-46% by volume		0.001 (high)	

<sup>\*</sup> Short term exposure limits

- 7.1.3 Made Ground can often contain degradable material such as wood, rags, paper and vegetation. However, the proportion of such carbon-rich materials is typically low, with major components often comprising re-worked clays, silts, sands and gravels, together with anthropogenic inclusions such as brick and concrete (CIRIA C665), as is anticipated to be the case at this site. A potential risk from ground gases was considered to be present, and further information was required to clarify this risk through intrusive ground investigation on site i.e. the composition of Made Ground, the potential for gas generation on site and the permeability of the strata.
- 7.1.4 Gas measurements were recorded from each monitoring borehole, on six separate occasions between 21 January and 26 February 2014. Atmospheric pressures were recorded between 979mb and 1004mb during the course of the monitoring visits. The full details of the ground gas monitoring are presented in Appendix D.

# 7.2 Assessment of Results

Tier 1 Ground Gas Risk Assessment

7.2.1 JPB uses the following generic screening levels to determine whether a potential risk exists:  $CH_4$  <1% by volume in boreholes, and  $CO_2$  <1.5% by volume in boreholes, providing borehole flow rates do not exceed 7l/h and 1.4l/h respectively.



- 7.2.2 H<sub>2</sub>S was only encountered in WS202 at a concentration of 1ppm during the first visit. There is currently little published guidance on the assessment of H2S for land use. The EH40/2005 'workplace exposure limits' guidance indicates a maximum exposure of 5ppm H<sub>2</sub>S over an eight hour reference period. The localised H<sub>2</sub>S concentration is significantly lower than this value on site, and it is stressed that this limit refers to a workplace and more confined area. It is noted that this was a single occurrence and is therefore not considered to be significant and requires no further assessment.
- 7.2.3 CH<sub>4</sub> was encountered during the third visit, at a concentration of 0.1% v/v in each of the three boreholes; at a concentration of 0.2% v/v in all three boreholes during the fourth visit, and in WS202 and WS205 during the sixth visit. As the JPB screening level for CH<sub>4</sub> is not exceeded, no further assessment of this gas is required.
- 7.2.4 CO was encountered at a concentration of 1ppm borehole WS205 during the fourth visit. There is currently little published guidance on the assessment of CO for residential land use. The EH40/2005 'workplace exposure limits' guidance indicates a maximum exposure of 30ppm CO over an eight hour reference period. The CO concentration encountered is significantly lower than this and are therefore not considered to be significant, and require no further assessment.
- 7.2.5 CO<sub>2</sub> was encountered in each monitoring well at least once during the monitoring visits. The recorded concentrations ranged from 0.2% v/v to 1.9% v/v. The maximum concentration was recorded in WS204 on the first visit. Therefore, as the screening concentration for CO<sub>2</sub> was exceeded, a more detailed Tier 2 Assessment for CO<sub>2</sub> is required.
- 7.2.6 The concentrations of  $O_2$  recorded in the boreholes during the monitoring period were at typical atmospheric conditions.
- 7.2.7 No significant gas flow has been recorded in the boreholes, with the maximum reading recorded at 0.4l/hr in borehole WS205 during the second visit.

#### Tier 2 Ground Gas Risk Assessment

- 7.2.8 On the basis of the redevelopment of the site for a residential use of unknown construction type, guidance provided in CIRIA C665 "Assessing Risks Posed by Hazardous Ground Gases to Buildings" has been referred to undertake the gas risk assessment. Extracts from this document are presented in Appendix D.
- 7.2.9 Carbon dioxide is heavier than air and tends to accumulate in confined spaces rather than flow. Sites with high gas concentrations and low flow rates are considered to be of a lower risk, when compared to sites with high flow rates and low concentrations (Wilson and Card, 1999).



- 7.2.10 The gas screening value (GSV) has been calculated using the maximum carbon dioxide concentration i.e. 1.9% by volume in WS204 and the worst case flow rate of 0.4l/hr from WS205. The conservative GSV is therefore calculated to be 0.0076l/hr (i.e. 0.019 x 0.4), which places the site in a Characteristic Situation 1 (CS1). This is considered to be 'very low risk' and as such no ground gas protection measures are required in buildings.
- 7.2.11 Whilst the assessment has classified a very low risk, the JPB CO<sub>2</sub> screening values have been exceeded and it should be noted that this preliminary assessment has been based on a limited number (six) of gas monitoring visits, during relatively high atmospheric pressures. Further gas monitoring visits are recommended in order to obtain ground gas data over a range of varying seasonal conditions to fully verify the ground gas regime on site.



#### 8.0 CHEMICAL RISK ASSESSMENT

# 8.1 Risk Assessment Approach

# Introduction

- 8.1.1 The UK framework for chemical risk assessment recently underwent significant change, with the Environment Agency withdrawing, in August 2008, the existing CLEA (Contaminated Land Exposure Assessment) framework. The current CLEA model, CLEA version 1.06, was released in October 2009, however; all of the withdrawn publications and supporting information have yet to be re-released.
- 8.1.2 On this basis, JPB's risk assessment approach is subject to alteration, to coincide with changes brought about through the release of documentation under the EA's programme of change. To this end, in the absence of certain data sets, guidance and supporting information, there is currently no single approach to assessing the risk to human health from soil contamination.

#### **Human Health**

- 8.1.3 The assessment of risk to human health can consider the potential for exposure based on comparison of the results from site specific ground investigation to conservative generic criteria.
- 8.1.4 Soil guideline values (SGVs) have been published by the EA for a limited number of determinands for a single soil type. SGVs are scientific; risk based generic assessment criteria for generic land use scenarios that can be used in the preliminary assessments of the risk to human health provided that the scenario is sufficiently representative of, or suitably conservative for, the conceptual site model. SGVs are currently published for eleven determinands; arsenic, cadmium, nickel, mercury, selenium, phenol, benzene, toluene, ethylbenzene, xylenes and dioxins, furans and dioxin-like PCBs.
- 8.1.5 The published SGVs are based on a sandy loam soil with 6% SOM (Environment Agency, 2009). If the soil at the site in question departs from the generic assumptions inherent in the SGV, three options are presented by the EA to the risk assessor:-
  - If the soil type is likely to be less protective of receptors, the risk assessor should derive a new GAC (generic assessment criteria) by adjusting the SGV for soil type and SOM. For example, a sandier, SOM-deficient soil is likely to provide less protection against exposure to volatile sources than that used in the derivation of the SGV.
  - If the soil type is likely to be more protective (for example a soil with a higher clay content and greater SOM for the same volatile source), or is sufficiently similar to the SGV assumption, the SGV can be used.
  - If the soil type is likely to be more protective, a new GAC (SAC) could be derived (particularly where the representative soil concentration of a chemical on a site exceed an SGV) by adjusting the SGV, thereby providing a less overly conservative screening tool.



- 8.1.6 Where the SGV is considered inappropriate to represent the site conditions, or where an SGV is not yet published for a determinand, soil assessment criteria (SAC) are derived for the site using CLEA Version 1.06 (released on 5 October 2009).
- 8.1.7 In view of the limited applicability of the published SGVs (in terms of relevant soils types), as part of this assessment, the published SGVs have not generally been adopted and SACs have been derived for the majority of common inorganic and organic analytical determinands using toxicological data from various sources, including the revised TOX Reports (arsenic, cadmium, nickel, mercury, selenium, phenol, benzene, toluene, ethylbenzene, xylenes and dioxins, furans and dioxin-like PCBs), the previously published TOX Reports (TOX 1 to 25) and the data obtained from the LQM / CIEH publication 2nd edition (2009) and the EIC/CLAIRE publication January 2010.
- 8.1.8 The TOX reports are currently being replaced on a rolling programme by the EA, as and when each new SGV report is published. The EA has stated "that much of the existing information in the TOX reports will not be affected by changes and will continue to be a useful interim resource until we make our new reports available" (EA website).
- 8.1.9 It should be noted that in assessing cadmium and its inorganic compounds in residential and allotment land uses, lifetime exposure should be considered. Although young children are generally more likely to have higher exposures to soil contaminants, the renal toxicity of cadmium are based on considerations of the kidney burden accumulated over 50 years or so (Environment Agency, 2009e). It is therefore reasonable to consider exposure not only in childhood but averaged over a longer time period. There is a facility within CLEA v1.06 to allow cadmium SACs to be generated based on lifetime exposure.
- 8.1.10 In the absence of a published SGV for lead, or the availability of toxicological data / standard input parameters which have been mutually agreed or accepted across the wider professional community (which would allow risk assessment using the CLEA version 1.06 model), JPB's current approach is to assess the risks from the recorded soil lead concentrations using the RISC4.0 model, referred to in more detail below. It is understood that Society of Brownfield Risk Assessment (SoBRA) is in the process of developing standard input parameters for use in the human health risk assessment of lead. However, these are yet to be made available.
- 8.1.11 Using the RISC4.0 model, risk estimates are compared with acceptability criteria at the risk evaluation stage in order to determine their significance for the dermal and ingestion pathways. It is considered that a Human Hazard Index (Quotient) in excess of 1.0, or an increased lifetime cancer risk in excess of one in one hundred thousand (10<sup>-5</sup>) are considered to be significant. Risk estimates for contaminants exceeding these criteria are considered to indicate that the contaminant poses a human health risk and that remedial action may be required to prevent actual harm.



- 8.1.12 The RISC4.0 modelling is compliant with the Risk Based Corrective Action (RBCA) philosophy and has been the subject of a comparative bench marking study carried out by the EA. Where the model allows, the input parameters have been adjusted to reflect the currently adopted UK approach. RISC4.0 is currently used to asses lead (as indicated above) and the chronic toxicity of cyanide. The acute toxicity of cyanide has been assessed using comparison to the worst case known fatal dose.
- 8.1.13 The soil modelling parameters calculated using both CLEA Version 1.06 and RISC4.0 are included in Appendix F, whilst further details of JPB's approach to risk assessment included in the Methodology for Exposure Assessment presented in Appendix G.

#### **Controlled Waters**

- 8.1.14 As with human health, the assessment of risk to controlled waters (surface waters and groundwaters) considers the potential for exposure based on comparison of the results, from the current JPB ground investigation, to conservative generic criteria.
- 8.1.15 Leachability analysis has been conducted on selected soil samples, in order to determine the likely mobility of the soil contaminants, and whether a threat to controlled waters exists. Leachate concentrations have been assessed against the criteria detailed below.
- 8.1.16 Groundwater samples are obtained, where encountered, to determine the existing concentrations within any perched waters or the underlying aquifer, which may have originated from either on site or potentially from off site sources. Groundwater concentrations are also assessed against the criteria detailed below.
- 8.1.17 Various Environmental Quality Standards (EQS) have been used to assess the concentrations of individual parameters identified in the leachate samples. The annual average EQS have been selected from EU Standards derived as part of the Water Framework Directive to protect surface water quality (inland waters) or from UK Standards established under the Dangerous Substances Directive (76/464/EEC), which are currently maintained under the Water Framework Directive. Predicted No Effect Concentration (PNEC) values are referred to for phenanthrene and pyrene, as there are currently no EQS values for these determinands. In addition, reference has been made to the Water Supply (Water Quality) (England and Wales) Regulations 2001 and 1989 and World Health Organisation (WHO) guidelines for drinking water, in the absence of EQS, or related EQS guidance, for specific determinands.
- 8.1.18 If any of the criteria described above are exceeded, for either human health or Controlled Waters, the conclusion is that a significant risk could exist, and further assessment is warranted, in order to calculate the potential levels of risk. This process therefore focuses on the parameters of concern and can inform upon any further investigations, which may be required for more detailed examination or remedial actions.



8.1.19 Further details of JPB's approach to risk assessment are presented in Appendix G - Methodology for Exposure Assessment. The chemical analysis certificates are presented in Appendix E.

# 8.2 Soil Chemical Analysis – Human Health

- 8.2.1 In deriving the GAC, this site has been assessed for a residential end use. On the basis of the findings of the previous desk study researches, it has been considered as one averaging area. The exposure pathways considered within this assessment include;
  - · Direct ingestion of soil and dust;
  - Direct ingestion of home grown produce;
  - Direct ingestion of soil on home grown produce;
  - Dermal contact with soil and dust (indoor and outdoor);
  - Inhalation of indoor and outdoor dust;
  - Inhalation of indoor and outdoor vapours.
- 8.2.2 The assessment has been based upon an end user considered to be the most conservative for a residential end use; a female child resident.
- 8.2.3 The soil properties have been selected as silty clay, with the pH and Soil Organic Matter (SOM) adjusted to reflect the actual site conditions of average pH 7.95 and a minimum SOM content of 0.96%. For the purposes of this assessment, site specific building parameters have not been entered. However, a 'semi-detached' house type has been used in the absence of any formal development proposals for the site.
- 8.2.4 The following determinands have been reported at or below the laboratory detection limits in every sample tested, and do not require any further assessment:
  - Phenols
  - Free cyanide
  - Total cyanide
  - Hexavalent chromium
  - Selenium
  - Aliphatic TPH C<sub>5</sub>-C<sub>44</sub>
  - Aromatic TPH C<sub>16</sub>-C<sub>21</sub>
  - Aromatic TPH C<sub>35</sub>-C<sub>44</sub>

- Benzene
- Toluene
- Ethylbenzene
- Xylenes
- MTBE
- Dibenz(a,h)anthracene
- PCB ICES 7 Congeners
- PCB WHO 12 Congeners
- 8.2.5 The soil concentrations of all the determinands encountered above the laboratory detection limits and assessed using the CLEA v1.06 model are all reported to be below the derived GAC for the specified use. The calculated GAC for the site are presented in Appendix F.



- 8.2.6 In the absence of generic criteria for human health risk assessment, the maximum total lead concentrations from the analysis detailed above have been assessed using the RISC4.0 model to provide a general indication of the potential risk to human health from lead encountered on site.
- 8.2.7 The RISC4 modelling of the dermal and ingestion pathways has been utilised to calculate the hazard indices and cancer risks to human health. Where a determinand has a risk exceeding that of the acceptability criteria; human hazard index >1 or increased cancer risk >10<sup>-5</sup>; it has been considered that a real risk exists. The RISC4 methodology is discussed in detail in Appendix G.
- 8.2.8 The assessment indicated that the cancer risk from the maximum of the general concentrations of lead found during the investigation is generally less than 1 in 100,000 and the human hazard index is less than 1.
- 8.2.9 Two soil samples submitted to the laboratory for chemical analysis were also subjected to an asbestos screen and identification test. Neither of these samples was determined as containing asbestos.
- 8.2.10 Reference to the UK Water Industry Research (UKWIR) document, "Guidance for the Selection of Water Supply Pipes to be used in Brownfield Sites", has been made and indicates that there may be contaminants on site which may restrict water pipe materials. In view of this, and on the basis of the UKWIR guidance, it is considered that chemical contamination present may permeate certain plastic water pipes and as such either wrapped ductile iron pipes with copper connectors or an approved PE-AI-PE barrier pipe system are recommended for potable water supplies.
- 8.2.11 It should be noted that the water company may require that a PID survey of the route of water supply pipes is undertaken, extending to 15m either side of the pipe route, in order to confirm that no unexpected chemical contamination is present. Alternatively, depending on the specific water supply company, this requirement can be satisfied by upgrading pipe materials to PE-AI-PE barrier pipe, which would be protective of water supplies. The water supply company responsible for the site should be consulted at the design stage of any redevelopment to confirm this.

# Summary

- 8.2.12 On the basis of the above, it is concluded that overall, the limited soil contamination identified on site does not present a significant risk to human health, in a residential scenario.
- 8.2.13 A copy of the certificates of analysis for all chemical laboratory analysis scheduled by JPB at the site is presented in Appendix E.



# 8.3 Groundwater Chemical Analysis – Controlled Waters

- 8.3.1 Groundwater was present in sufficient volumes to obtain representative samples for laboratory analysis from one borehole, WS202. The results have been assessed against the Tier 1 criteria, as described previously, based on the site's environmental setting.
- 8.3.2 The following determinands have been reported at, or below, the laboratory detection limits in every sample tested, and do not require any further assessment:
  - MTBE
  - Total cyanide
  - · Free cyanide
  - Sulphide
  - Lead
  - Beryllium
  - Cadmium
  - Chromium
  - Hexavalent chromium
  - Nickel
  - Mercury

- Vanadium
- Phenols
- USEPA 16 PAH
- PCB CLEA 12 Congeners
- PCB ICES 7 Congeners
- Benzene
  - Toluene
- Ethyl benzene
- Xylenes
- Aliphatic and Aromatic TPH C<sub>5</sub>-C<sub>44</sub>

8.3.3 None of the concentrations of the determinands encountered above the laboratory detection limits were in excess of the Tier 1 criteria.

#### Summary

- 8.3.4 Based on the laboratory analysis, it is concluded that limited determinands encountered in the groundwater are likely to be attributable to the low level determinands present within the soil. However, given the low concentrations and no exceedances of the assessment criteria together with the localised nature of the groundwater, it is considered unlikely that these contaminants present a significant risk to local controlled waters, either groundwater or surface waters. It is concluded that the elevated determinands recorded within the groundwater do not present a significant risk to controlled waters.
- 8.3.5 A copy of the certificates of analysis for all chemical laboratory analysis scheduled by JPB at the site is presented in Appendix E.

#### 8.4 Waste Classification

8.4.1 In addition to considering the potential risk from contamination on site to human health and the environment, an assessment of the waste classification has been undertaken. The assessment has been completed using the CAT-WASTE SOIL service provided by Atkins.



8.4.2 All of the soil results from the site were submitted and the resulting assessment has confirmed that soils tested in this investigation would not be classified as hazardous waste should they be removed for off site disposal. The CAT-WASTE SOIL output sheet is presented in Appendix F.



#### 9.0 CONCLUSIONS AND RECOMMENDATIONS

#### 9.1 Conclusions

- 9.1.1 A Phase 2 Intrusive Ground Investigation has been carried out by JPB at the site known as 12 and 14 Edhill Avenue and is the subject of this report. This report has been written for STH and is required in order to determine the shallow and general ground conditions on site. This report also highlights any potential environmental risks and liabilities associated with the future redevelopment of the site, arising from its past and present uses. At the time of writing, it is understood that STH is considering the redevelopment of the site for residential use, although no detailed proposals have been determined.
- 9.1.2 The shallow Made Ground deposits were noted to be highly variable in terms of thickness, composition and strength across the site and are not generally considered appropriate for use as a founding medium. The underlying Pelaw Clay derived cohesive strata are broadly considered acceptable for founding purposes. The Pelaw Clay materials would be classified as 'low' volume change potential materials under the NHBC guidance using their 'modified' plasticity indices. As such, a minimum founding depth of 1.0m bgl will be applicable assuming restricted new planting or the presence of existing trees or vegetation within influencing distance of the future foundations. Outside the zone of influence of any proposed or existing trees or vegetation the minimum founding depth will be 0.75m bgl provided that a suitable foundation stratum exists at this level.
- 9.1.3 Assuming a founding depth of 1.0m bgl a maximum net allowable bearing pressure of 80kNm<sup>-2</sup> is considered appropriate for future foundations, so as to limit settlement to less than 25mm. Conventional strip footings are considered appropriate for use for up to two storey traditional brick built structures. Should higher bearing pressures be required then it may be necessary to adopt semi-raft style foundations so as to spread the imposed structural loads over a larger area.
- 9.1.4 For the purpose of designing sub-surface concrete to BS EN 206-1/BS50, guidance has been obtained from BRE SD1:2005 "Concrete in Aggressive Ground". The site has been classified as 'brownfield with static groundwater' based upon the guidance documentation. The site classifies under the guidance as DS-1 and classifies the ACEC class of the site as AC-1s, as derived from Table C2 in BRE SD1:2005. This corresponds to a Design Chemical Class (DC) of DC-1 assuming a designed working life of 100 years.
- 9.1.5 The various intrusive investigations indicate that the geology at this site is **not** suited to the use of infiltration style drainage for the collection and disposal of run-off waters.



- 9.1.6 Based on the preliminary gas risk assessment, the gas screening value (GSV) has been calculated using the maximum carbon dioxide concentration i.e. 1.9% by volume in WS204 and the worst case flow rate of 0.4l/hr from WS205. The conservative GSV is therefore calculated to be 0.0076l/hr (i.e. 0.019 x 0.4), which places the site in a Characteristic Situation 1 (CS1). This is considered to be 'very low risk' and as such no ground gas protection measures are required in buildings.
- 9.1.7 It is concluded that overall, the limited soil contamination identified on site does not present a significant risk to human health, in a residential scenario.
- 9.1.8 The groundwater assessment has confirmed that limited determinands are [present in the groundwater, although not in excess of assessment criteria. It is concluded that the elevated determinands recorded within the groundwater do not present a significant risk to controlled waters.
- 9.1.9 An assessment has been completed using the CAT-WASTE<sup>SOIL</sup> service provided by Atkins. All of the soil results from the site were submitted and the resulting assessment has confirmed that soils tested in this investigation would not be classified as hazardous waste should they be removed for off site disposal.
- 9.1.10 Reference to the UK Water Industry Research (UKWIR) document, "Guidance for the Selection of Water Supply Pipes to be used in Brownfield Sites", has been made and indicates that there may be contaminants on site which may restrict water pipe materials. In view of this, and on the basis of the UKWIR guidance it is considered that chemical contamination present may permeate certain plastic water pipes and as such either wrapped ductile iron pipes with copper connectors or an approved PE-AI-PE barrier pipe system are recommended for potable water supplies.

#### 9.2 Recommendations

- 9.2.1 Whilst the assessment has classified a very low risk, the JPB CO<sub>2</sub> screening values have been exceeded and it should be noted that this preliminary assessment has been based on a limited number (six) of gas monitoring visits, during relatively high atmospheric pressures. Further gas monitoring visits are **recommended** in order to obtain ground gas data over a range of varying seasonal conditions to fully verify the ground gas regime on site.
- 9.2.2 It is **recommended** that once a development layout is available that the proposed foundation design is considered on a 'per plot' basis and a Foundation Schedule prepared giving details of foundation type, type of ground improvement etc. Given the variation in terms of composition, strength and thickness of the shallow soils this may result in a more economic design than considering the site as a 'whole'. JPB would be pleased to assist in the preparation of a Foundation Schedule once a development plan has been prepared.

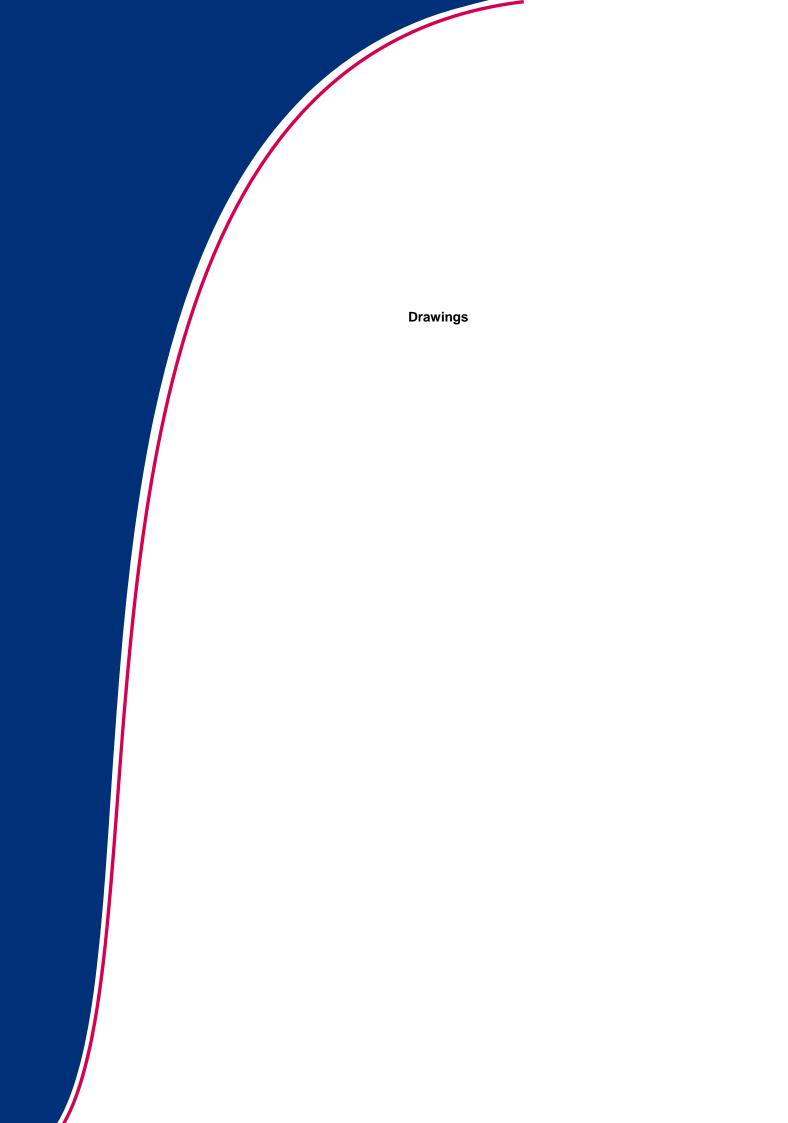


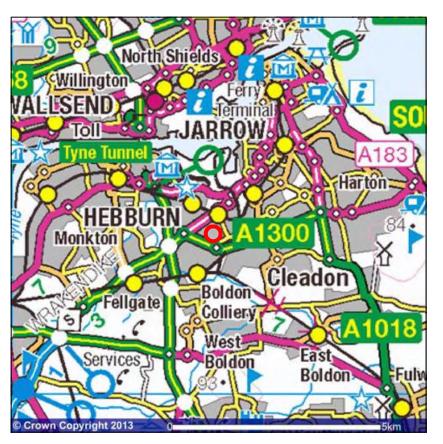
- 9.2.3 Intrusive investigation indicates that the geology at this site is **not likely to be suited** to the use of infiltration style drainage for the collection and disposal of run-off waters. As such, it is considered that **attenuation storage will have to be provided** to allow the proposed development to meet its obligations under PPS25. Attenuation storage could take the form of increased thicknesses of sub-base beneath hardstanding or by providing 'crated' attenuation cells beneath hardstanding or in garden areas.
- 9.2.4 The water supply company responsible for the site **should be consulted** at the design stage of any redevelopment to confirm whether specialist materials will be required for water supply pipes.
- 9.2.5 The recycling and reuse of materials on site should be promoted wherever possible to reduce waste. Therefore, during development, validation testing should be carried out on the materials to ensure their suitability in terms of chemical and physical characteristics. Any imported materials should also be subject to chemical and physical analysis to ensure that they are fit for use on site.
- 9.2.6 All soils for disposal require pre-treatment, which may involve screening, sorting or chemical treatment, for example, to promote the reduction in volume of wastes being landfilled, to promote recycling and/or to render materials more chemically inert. Any materials requiring off site disposal are likely to be classified as non-hazardous / inactive wastes, although it is **recommended** that confirmation of this is sought from the local landfill operator.



#### 10.0 GENERAL

- 10.1 Whilst confident in the findings of our report we are unable to give an assurance that they will be accepted by the authorities without question. We therefore advise that where appropriate our report and associated matters are submitted to approving bodies and approval obtained or sought before detailed design, site works or other irrevocable action is embarked upon.
- 10.2 The recommendations contained in this report do not constitute any form of specification for the undertaking of the works required.
- 10.3 It should be noted that soil and rock conditions are highly variable and may differ between sampling points and this may affect interpolation. Additionally features may exist buried at depth and undetected by investigation. Other information may become available on the conditions of the site not available at the date of this report and thus site assessment may be subject to amendment in the light of such additional information becoming available.
- 10.4 The conclusions reached in this report are necessarily restricted to those that can be determined from the information consulted and may be subject to amendment in the light of additional information becoming available.
- 10.5 This report and related documents have been prepared for the sole use of the specified client in response to an agreed brief, for a stated purpose and at a particular time and its application must be made accordingly. No duty of care extends to any other party who may make use of the information contained therein
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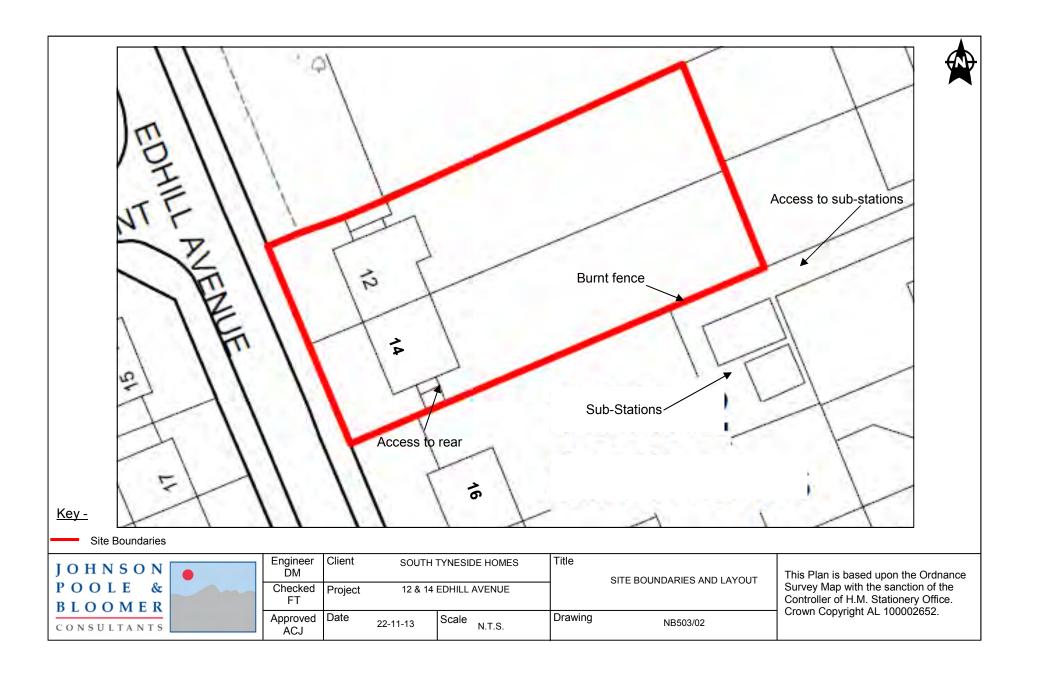
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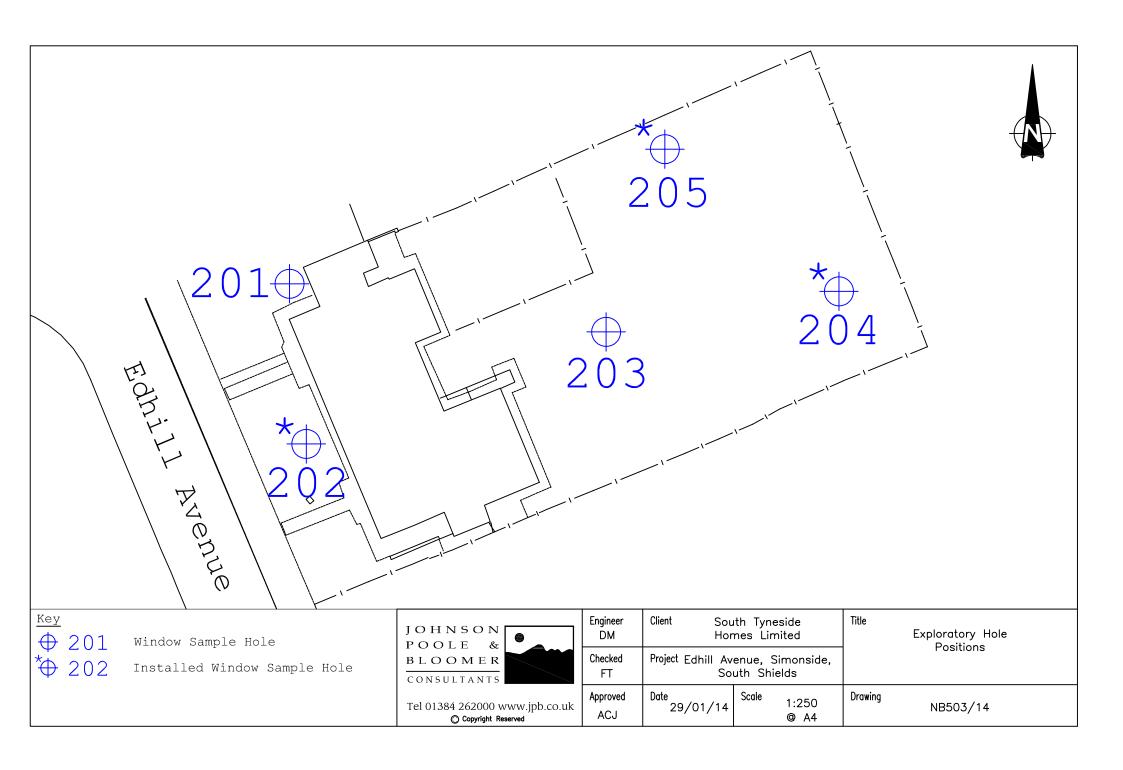


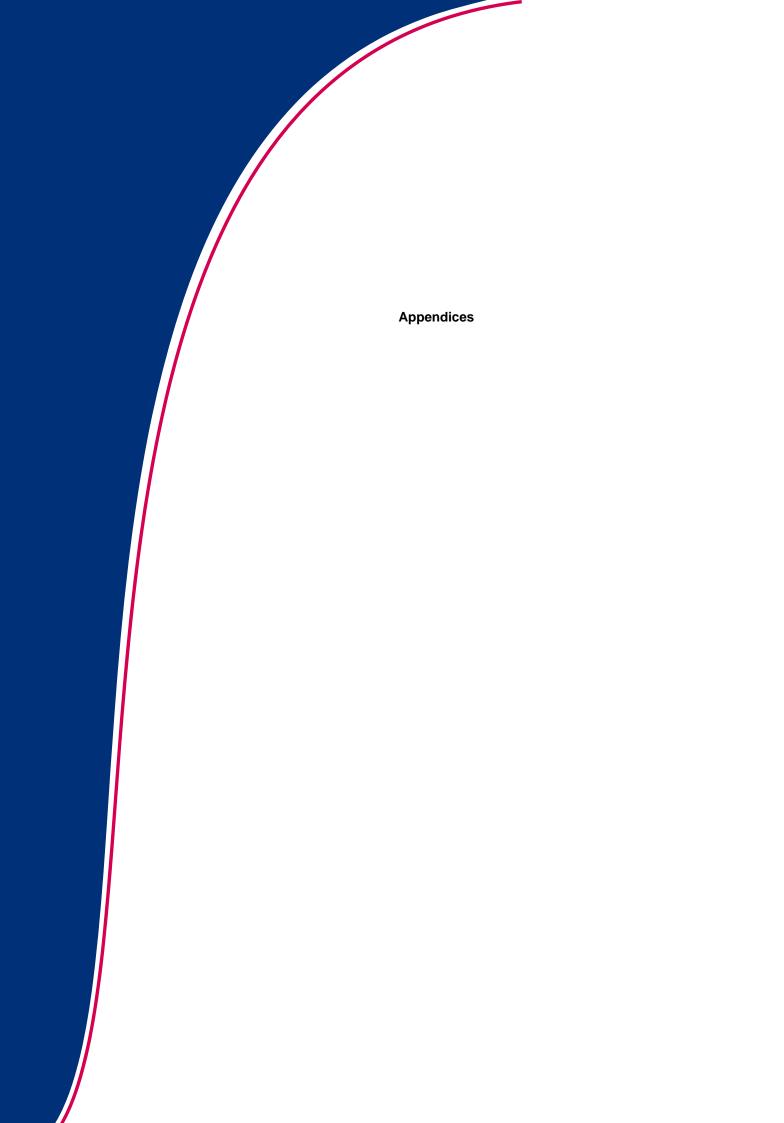


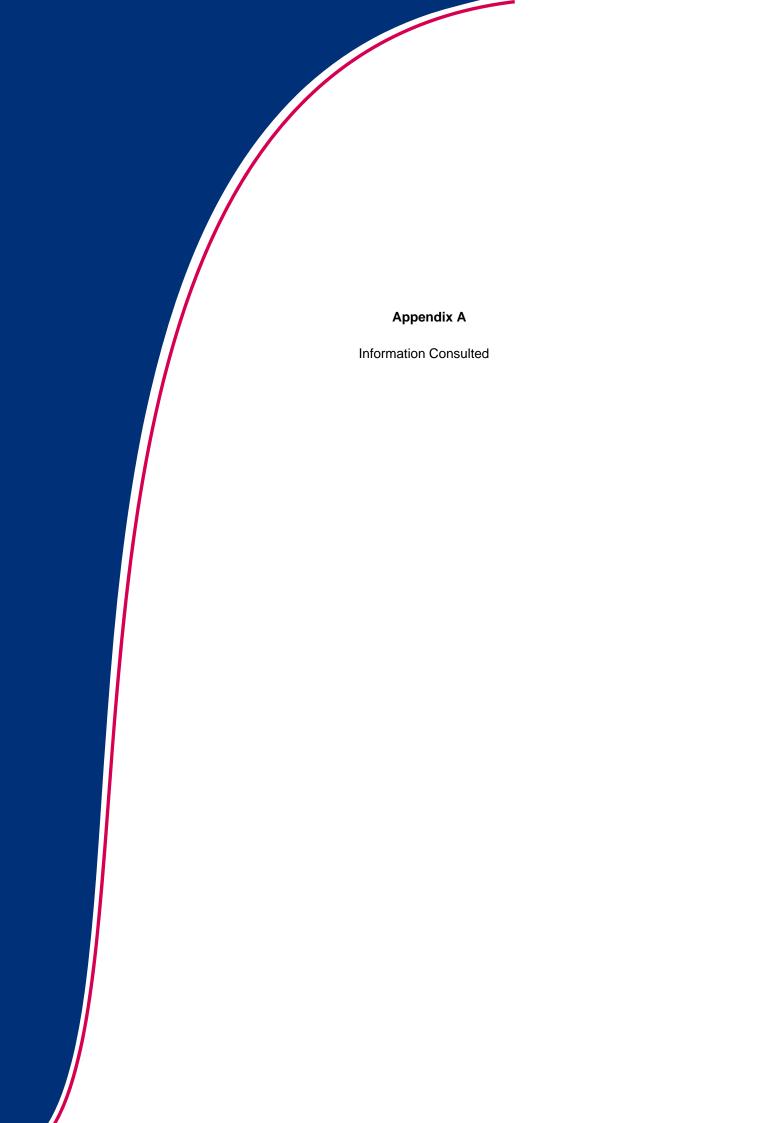
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#### INFORMATION CONSULTED:

In preparation of this report, the following information has been consulted:

#### General

- JPB Archive
- Historical Ordnance Survey Plans
- Coal Authority Gazetteer, Law Society Guidance Notes and Directory of Coal Mining Searches 2006

#### **Environmental Setting**

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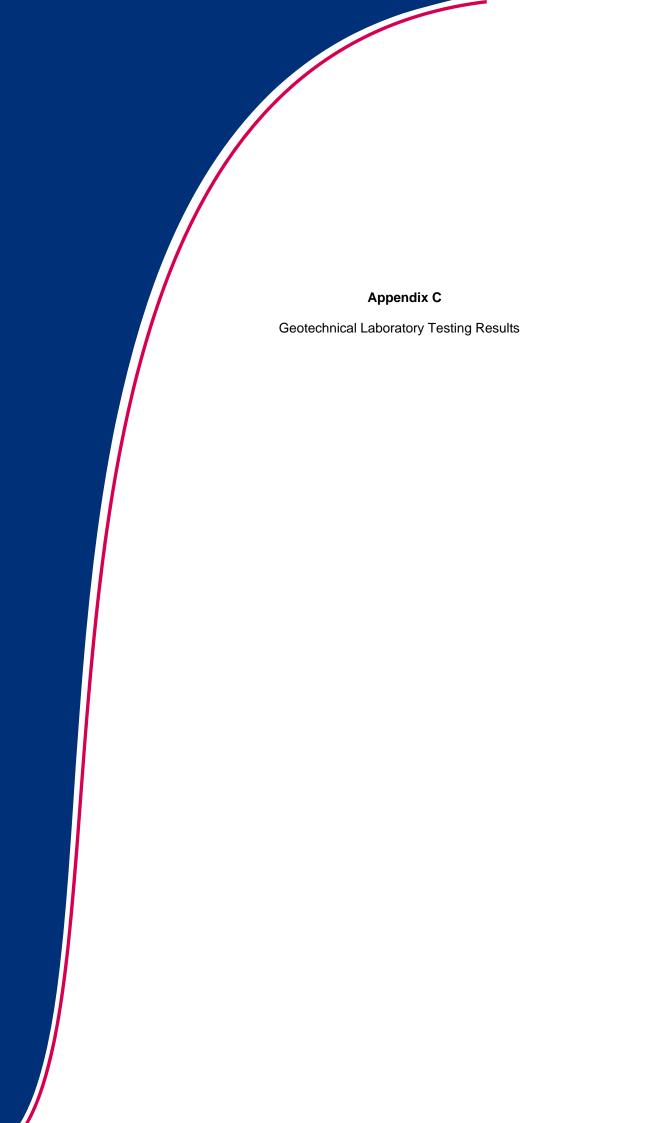
<b>i</b>	JOHNSON POOLE & BLO			OME	ER AGS	Site Edhill Avenue, Simonside, South Shields		Number 201
Excavation Drive-in Win	Method dow Sampler	83	sions 11mm to 1.00m 1mm to 2.00m 1mm to 4.00m		<b>Level (mOD)</b> 24.10	Client South Tyneside Homes Ltd		Job Number NB503-E
		<b>Locatio</b> Se	ee JPB drawing NB503/14	Dates 09	9/01/2014	Engineer Johnson Poole & Bloomer Ltd		Sheet 1/1
Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description		Vater Variet
0.20	D1			23.65	(0.45)	MADE GROUND: Grass over dark brown clayey slig gravelly SILT. Gravel sized fragments of sub angula coarse brick, concrete and quartzite. Many roots and rootlets. Occasional cobbles of brick. Firm to stiff mid brown mottled light grey slightly gra CLAY. Gravel of sub rounded fine and medium coal	d 	
0.70	EA		Slow(1) at 0.80m.			quartzite, mudstone and sandstone.	, quariz,	<u>`</u>
1.20-1.65 1.20	SPT N=14 D2		3,3/3,4,4,3		(1.55)			
1.90 1.90 2.00-2.45 2.20	V1 60 kN/m2 V2 70 kN/m2 D3 SPT N=17 D4		3,3/3,4,4,6	22.10	2.00	Dark brown gravelly CLAY. Gravel of sub rounded fill medium coal, quartzite, mudstone and sandstone.	ne and	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2.70	V3 65 kN/m2				<u>-</u> - - - -			0 0 0 0
3.00-3.45	SPT N=18		3,3/3,4,5,6					
3.50 3.50	V4 65 kN/m2 D5							
3.90 4.00-4.45	V5 65 kN/m2 SPT N=11		2,2/2,3,3,3		(4.45)			
5.00-5.45	SPT N=12		2,2/2,3,3,4		<u>-</u>     			
5.50	V6 55 kN/m2							
6.00-6.45	SPT N=15		2,2/3,3,4,5		<u>-</u> - - - - - - -			0 0 0
				17.65	6.45	Complete at 6.45m		<u> </u>
A slow inflow Upon comple	v of groundwater was etion exploratory hole	encounte was back	kfilled with lightly compacted n		ngs.		Scale (approx)	Logged By
v = Hand he Exploratory h	eru snear vane, E = Er hole completed at 6.4	Ivironmer I5m on the	ntal sample, D = Disturbed sar e instruction of JPB Engineer.	пріе		-	1:40 Figure N	
i							NR2(	03.201

<b>i</b>	OHNSO	N PC	OOLE & BLC	OMI	ER	AGS	Site Edhill Avenue, Simonside, South Shields			lumb <b>20</b> 2	
Excavation Drive-in Win	<b>Method</b> dow Sampler	83	sions 11mm to 1.00m mm to 2.00m mm to 4.00m	Ground	<b>Level</b> 22.25	(mOD)	Client South Tyneside Homes Ltd		Ň	ob lumb	-
		<b>Locatio</b> Se	e JPB drawing NB503/14	Dates 09	9/01/20	14	Engineer  Johnson Poole & Bloomer Ltd		s	1/1	
Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	De (I (Thic	epth m) kness)	Description	Legend	Water	Ins	str
0.30 0.30	EA D1		Very slow(1) at 0.60m.	21.85	E	(0.40)	MADE GROUND: Grass over soft dark brown slightly silty slightly gravelly CLAY. Gravel sized fragments of sub rounded and sub angular fine an medium mudstone, brick and concrete. Many roots and rootlets. Metal bar 0.3m in length at 0.25m bgl Firm light brown mottled light grey slightly gravelly CLAY. Gravel of sub rounded to rounded fine and medium quartz and quartzite.		- <b>V</b> 1		
1.20-1.65 1.40	SPT N=15 D2		4,3/3,3,4,5	20.65	الململململ	1.60	Firm chocolate brown slightly gravelly CLAY. Gravel of sub rounded fine to coarse sandstone,		- - - - -		
1.90 2.00-2.45 2.20	V1 45 kN/m2 SPT N=20 EB		3,3/4,5,5,6				mudstone, coal and quartzite. Occasional cobble of quartzite.	)f			
2.60 2.70 2.80 3.00-3.45 3.30	V2 70 kN/m2 D3 V3 70 kN/m2 SPT N=18 V4 75 kN/m2		3,4/4,4,4,6		ليبينينانينينيانيينا			0   0   0   0   0   0   0   0   0   0	- - - -		
4.00-4.45 4.40	SPT N=13		2,2/3,3,3,4			(5.85)			-		
5.00-5.45	SPT N=15		3,3/4,3,3,5		بتناءيتين أيتينين	(0.00)			- - - -		
6.00-6.45	SPT N=16		3,3/3,4,4,5						     		
6.50 6.50	V5 65 kN/m2 D5								-		
7.00-7.45	SPT N=13		2,2/3,3,3,4	14.80	سنطيسان	7.45		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- - - -		
Remarks		<u> </u>			<u>E</u> _			Scale	<u> </u>	ogg	
A very slow i Upon comple to 0.50m pla	nflow of groundwater etion exploratory hole in pipe with bentonite	was enco installed surrounce	1 0 50m to 1 50m slotted pipe	e with gravel	nitoring surrou	standp	ipe. GL to 0.10 metal cover set in concrete, 0.10 1.50m to 7.45m backfilled with natural arisings.	Scale (approx)	B	ogge y DM	
V = Hand he	ld shear vane, $E = Er$	nvironmer	ntal sample, D = Disturbed sa e instruction of JPB Engineer	ımple				Figure N	<b>No.</b> 503.2		

<b>i</b>	JOHNSON POOLE & BLO			OME	ER AGS	Site Edhill Avenue, Simonside, South Shields		Numbe	
Excavation Drive-in Win	Method dow Sampler	83	ions 1mm to 1.00m mm to 2.00m mm to 4.00m		<b>Level (mOD)</b> 22.21	Client South Tyneside Homes Ltd		Job Numbe NB503	
		<b>Locatio</b> Se	n ee JPB drawing NB503/14	Dates 09	/01/2014	Engineer Johnson Poole & Bloomer Ltd		Sheet 1/1	
Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description		Legend	Water
				21.91	(0.30)	MADE GROUND: Grass over soft dark brown to grey silty CLAY. Occasional gravel sized fragments of sub angular fine brick, sandstone and quartzite.			
0.70	D1		Very slow(1) at 0.80m.		.1.1.1.1.1	Firm to stiff light brown mottled grey gravelly CLAY. Gof sub angular fine sandstone, coal and quartzite.	Gravel		<b>V</b> 1
1.10 1.20-1.65	EA SPT N=13		2,2/3,3,3,4		(1.70)				
1.50 1.60	V1 104 kN/m2 D2								
1.90 2.00-2.45	V2 120+ kN/m2 SPT N=19		2,3/3,4,5,7	20.21	2.00	Stiff chocolate brown slightly gravelly CLAY. Gravel or rounded fine to coarse sandstone, coal and quartzite. cobble of sandstone.	of sub . Rare		
2.50 2.70 2.80 2.90 3.00-3.45	V3 104 kN/m2 EB D3 V4 94 kN/m2 SPT N=19		3,3/4,4,5,6		المستملسين المستمالة				
4.00-4.45	SPT N=16		2,3/3,4,4,5		(4.45)				
4.50 4.70	D4 V5 70kN/m2							0 0 0	
5.00-5.45	SPT N=16		2,2/4,4,3,5						
5.55-6.00	U1								
6.00-6.45	SPT N=16		2,2/3,3,4,6		<u></u>				
				15.76	6.45	Complete at 6.45m			
A very slow i	inflow of groundwater etion exploratory hole	was ence	to drilling by JPB Engineer. ountered at 0.80m bgl. kfilled with lightly compacted n	natural arisin	ngs.		Scale (approx)	Logged By	d
V = Hand he Exploratory h	ld shear vane, É = En nole completed at 6.4	nvironmer 15m on the	ntal sample, D = Disturbed san e instruction of JPB Engineer.	nple, U = U	ndisturbed sa	mple	1:40 Figure N		
1							NB50	03.203	

<b>i</b>	OHNSO	N PC	OOLE & BLC	OMI	ΞR	AGS	Site Edhill Avenue, Simonside, South Shields		N	lumber 204
Excavation Drive-in Win	Method dow Sampler	l 83	ions 1mm to 1.00m mm to 2.00m mm to 4.00m	Ground	<b>Leve</b> 22.04	. ,	Client South Tyneside Homes Ltd		N	ob lumber NB503-E
		<b>Locatio</b> Se	e JPB drawing NB503/14	Dates 09	9/01/20	014	Engineer  Johnson Poole & Bloomer Ltd		s	Sheet 1/1
Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	D (Thi	epth (m) ckness)	Description	Legend	Water	Instr
0.40 0.60 1.20-1.65 1.40 1.50 1.90 2.00-2.45 2.45 2.55-3.00 3.00-3.45 3.50 3.70 3.80 4.00-4.45 4.50 4.80 5.00-5.45	EA D1  SPT N=13 D2 V1 120+ kN/m2  V2 120+ kN/m2 SPT N=25  V3 108 kN/m2 U1  SPT N=19  D3 V4 70 kN/m2 EB SPT N=13  V5 72 kN/m2 D4 SPT N=13  V6 64 kN/m2  SPT N=21		2,2/2,3,4,4  5,4/6,6,6,7  3,4/4,5,4,6  2,2/3,3,3,4  2,3/3,3,3,4	21.59		(0.45) 0.45 (0.55) 1.00	MADE GROUND: Grass over slightly clayey SILT. Occasional gravel sized fragments of sub angular fine to medium coal, brick, mudstone and concrete.  Stiff light brown mottled light grey slightly gravelly CLAY. Gravel of sub rounded fine to medium sandstone, mudstone, quartzite and coal.  Stiff chocolate brown gravelly CLAY. Gravel of sub rounded fine to coarse sandstone, coal, mudstone and quartzite. Occasional cobble of quartzite.		\tag{\text{\tin}\exitt{\text{\tin}\xi}\\ \text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\tex{\tex	
Groundwate Upon compl	r was not encountere etion exploratory hole	d during of installed	with combined gas and groun	ndwater more with gravel	nitorin	g standp und and	ipe. GL to 0.10 metal cover set in concrete, 0.10 3.00m to 6.45m backfilled with natural arisings. nple	Scale (approx)		ogged DM
v = Hand he Exploratory l	nd snear vane, E = Er nole completed at 6.4	ivironmer 5m on the	ntal sample, D = Disturbed sa e instruction of JPB Engineer.	ırıpıe, U = U	ındıstı	irded sar	npie -	Figure I	<b>No.</b> 503.2	204

<b>i</b>	OHNSO	N PC	OOLE & BLC	ОМІ	ER	AGS	Site Edhill Avenue, Simonside, South Shields		1	umber <b>205</b>	
Excavation Drive-in Win	Method dow Sampler	83	ions 1mm to 1.00m mm to 2.00m mm to 4.00m	Ground	<b>Level</b> ( 22.20	(mOD)	Client South Tyneside Homes Ltd		N	ob umber IB503-I	
		<b>Locatio</b> Se	e JPB drawing NB503/14	Dates 09	9/01/20 <sup>-</sup>	14	Engineer  Johnson Poole & Bloomer Ltd		S	<b>heet</b> 1/1	
Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	De (r (Thicl	epth m) kness)	Description	Legend	Water	Instr	ſ
0.30	D1			21.70	E	(0.50) 0.50	MADE GROUND: Grass over dark brown clayey SILT. Occasional gravel sized fragments of sub angular fine glass, brick, quartzite and quartz.  Firm to stiff light brown mottled light grey slightly gravelly CLAY. Gravel of sub rounded fine and				
0.90 1.00 1.20-1.65 1.30 1.40	EA D2 SPT N=13 V1 110+ kN/m2 D3		1,2/2,3,3,5			(1.80)	medium sandstone, mudstone, coal and quartzite. Occasional fine rootlets.				
1.90 2.00-2.45	V2 110+ kN/m2 SPT N=18		3,3/4,4,4,6	19.90	التليليليليليليل	2.30	Stiff mid brown gravelly CLAY. Gravel of sub rounded fine to coarse coal, mudstone, sandstone,				
2.70	D4			19.20	Ē	3.00	quartzite and quartz. Occasional cobble of quartzite.				× ×
3.80 3.90 4.00-4.45	D5 V3 99 kN/m2 SPT N=16		2,3/3,4,4,5	10.20		0.00	Firm mid brown gravelly CLAY. Gravel of coal, mudstone, sandstone, quartzite and quartz. Frequent cobbles of quartzite from 5.0m.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
4.55-5.00	U1					(3.45)					
5.00-5.45 6.00-6.45	SPT N=34  SPT N=14		3,3/6,4,4,20 2,2/2,3,4,5		المالمالمالمالمالمالمالمالمالمالمالمالما				-		
				15.75	انتينينيانينينيانيينينايين	6.45	Complete at 6.45m	\$ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
Groundwate Upon comple	r was not encountere etion exploratory hole	d during of installed	with combined gas and grou				ipe. GL to 0.10 metal cover set in concrete, 0.10	Scale (approx)	F	ogged y	
V = Hand he Exploratory h	ld shear vane, E = Er nole completed at 6.4	nvironmer 5m on the	I, 0.50m to 2.00m slotted pipe ttal sample, D = Disturbed sa e instruction of JPB Engineer ed to have been increased di	ample, Ŭ = U	Indistur	bed sar		1:40 Figure N	<b>No.</b> 503.2	DM 205	







## Contract Number: 22129

Client's Reference: NB503-E PO5616 Report Date: 07-02-2014

Client Johnson Poole & Bloomer (Midlands)

**Harris & Pearson Building** 

**Brettell Lane Brierley Hill West Midlands** 

DY5 3LH

Contract Title: Edhill Avenue, South Tyneside

For the attention of: Julian Charlesworth

Date Received: 27-01-2014 Date Commenced: 27-01-2014 Date Completed: 07-02-2014

4 Point Liquid & Plastic Limit (LL/PL)	3.0
<b>Moisture Content</b> 1377 : 1990 Part 2 : 3.2 - UKAS *	3.0
Test Description	Qty

Notes: Observations and Interpretations are outside the UKAS Accreditation

\* - denotes test included in laboratory scope of accreditation

# - denotes test carried out by approved contractor

This certificate is issued in accordance with the accreditation requirements of the United Kingdom Accreditation Service. The results reported herein relate only to the material supplied to the laboratory. This certificate shall not be reproduced in full, without the prior written approval of the laboratory.

Approved Signatories:

Alex Wynn (Associate Director) - Benjamin Sharp (Contracts Manager) - Emma Williams (Office Manager) Paul Evans (Quality/Technical Manager) - Vaughan Edwards (Managing Director)

Unit 4, Heol Aur, Dafen Ind Estate, Dafen, Llanelli, Carmarthenshire SA14 8QN

1377: 1990 Part 2: 4.3 & 5.3 - UKAS \*

Client ref: NB503-E

Location: Edhill Avenue, South Tyneside

Contract Number: 22129-270114

Number Number Number Type Depth (m)  201 D 2.20 Brown fine to medium gravelly slightly sandy slity CLAY. 203 D 0.70 Brown fine to medium gravelly slightly sandy slity CLAY.  205 D 1.40 Brown fine to medium gravelly slightly sandy slity CLAY.  Brown fine to medium gravelly slightly sandy slity CLAY.	<del></del>				
Depth (m)  Brown fine to medium gravelly slightly sandy silty CLAY.  Depth (m)  Depth (m)  Brown fine to medium gravelly sandy silty CLAY.		Sample	_		
D 2.20 Brown fine to medium gravelly slightly sandy silty CLAY.  D 0.70 Brown fine to medium gravelly sandy silty CLAY.	Number	Number	Туре		Description of Sample*
D 0.70 Brown fine to medium gravelly sandy silty CLAY.				Depth (m)	
203 D 0.70 Brown fine to medium gravelly sandy silty CLAY.  205 D 1.40 Brown fine to medium gravelly slightly sandy silty CLAY.  206 C 1.40 C	201		D	2.20	Brown fine to medium gravelly slightly sandy silty CLAY.
205 D 1.40 Brown fine to medium gravelly slightly sandy silty CLAY.	203		D	0.70	Brown fine to medium gravelly sandy silty CLAY.
	205		D	1.40	Brown fine to medium gravelly slightly sandy silty CLAY.

Note: Results on this table are in summary format and may not meet the requirements of the relevant standards, additional information is held by the laboratory

GS STEEL STREET SERVICES LIMITED

Checked By

Approved By:

Date Approved: 7

7.2.14

Test Report: Method of the Determination of the plastic limit and plasticity index

BS 1377: Part 2: 1990 Method 5

Client ref: NB503-E

Location: Edhill Avenue, South Tyneside

Contract Number: 22129-270114

Hole/			Moisture	Liquid	Plastic	Plasticity	%	
Sample	Sample	Depth	Content	Limit	Limit	Index	Passing	Remarks
Number	Туре	m	%	%	%	%	.425mm	
			CI. 3.2	CI. 4.3/4.4	CI. 5.	CI. 6.		
201	D	2.20	17.3	37	20	17	85	CI Intermediate Plasticity
203	D	0.70	33.8	48	24	24	81	CI Intermediate Plasticity
205	D	1.40	15.5	40	16	24	78	CI Intermediate Plasticity

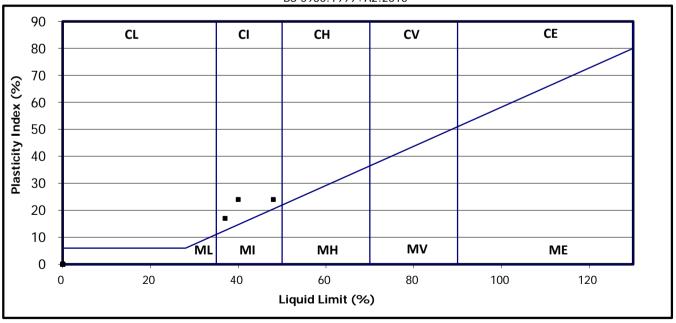
Symbols:

NP : Non Plastic #

#: Liquid Limit and Plastic Limit Wet Sieved

PLASTICITY CHART FOR CASAGRANDE CLASSIFICATION.

BS 5930:1999+A2:2010





Checked By

Approved By:



Date Approved: 7.2.14





JPB GAS MONITORING DATA								
Site Name Edhill Avenue, Simonside, South Shields Project Number								
Project Manager	Fiona Townley	NB503						

### **INSTRUMENTATION**

## **GAS CONCENTRATIONS**

	VISIT 1	VISIT 2	VISIT 3	VISIT 4	VISIT 5	VISIT 6
Geotech Instruments GA5000	✓	✓	✓	✓	✓	✓
Geotech Instruments GA2000						

### **GAS FLOW**

Geotech Instruments Inbuilt Flow Pod	✓	✓	✓	✓	✓	✓
Geotech Instruments Flow Pod						

Date	21/01/2014	Weather	Sunny but cold with falling pressure				
Engineer	DM	Atmospheric	Pressure	1004			



Gas Read Borel		20	02		e level OD)			Comm	ents			
Time	CH₄ %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H₂S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.3	20.4		0	0	1004	-0.07	0	0.72	1.57	
30s	0.0	0.3	20.3		0	0			0.1			
60s	0.0	0.3	20.4		1	0			0.1			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Gas Read Borel		20	04		e level OD)			Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.2	20.7		0	0	1004	-0.14	0	Dry	2.99	
30s	0.0	1.9	19.4		0	0			0.1			
60s	0.0	1.9	19.0		0	0			0.2			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Gas Read Borel		20	05		e level OD)			Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.3	20.5		0	0	1004	-0.14	0	Dry	2.1	
30s	0.0	1.1	19.8		0	0			0.1			
60s	0.0	1.1	19.6		0	0			0.1			
90s									0.1			
120s									0.1			
150s									0.1			
180s									0.1			
210s												
240s												
270s												
300s												

Date	27/01/2014	Weather	Cloudy and cold	with level pressure
Engineer	DM	Atmospheric	Pressure	979



Gas Read Borel		20	02		e level			Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.3	20.6		0	0	979	0.21	0	0.85	1.6	
30s	0.0	0.3	20.6		0	0			0.2			
60s	0.0	0.2	20.6		0	0			0.2			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Gas Read Borel		20	04		e level OD)			Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.2	20.5		0	0	979	0.09	0	Dry	2.99	
30s	0.0	1.8	19.3		0	0			0.1			
60s	0.0	1.8	19.3		0	0			0.2			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Gas Read Borel		20	205		Surface level (mAOD)			Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.3	20.6		0	0	979	0.03	0	0.65	2.09	
30s	0.0	1.0	20.0		0	0			0.2			
60s	0.0	1.0	20.0		0	0			0.4			
90s									0.4			
120s									0.4			
150s									0.4			
180s									0.4			
210s												
240s												
270s												
300s												

Date	04/02/2014	Weather	Overcast and cold	with falling pressure
Engineer	DM	DM Atmospheric Pressu		992



Gas Read Borel		20	02	Surfac (mA	e level OD)			Comm	ents			
Time	CH₄ %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H₂S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.1	0.2	20.9		0	0	992	0.05	0	0.88	1.6	
30s	0.1	0.3	20.9		0	0			0.2			
60s	0.1	0.2	20.9		0	0			0.3			
90s									0.3			
120s									0.3			
150s									0.3			
180s									0.3			
210s												
240s												
270s												
300s												

Gas Read Borel		20	04		e level OD)			Comm	ents			
Time	CH₄ %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.1	0.2	20.8		0	0	992	0.17	0	0.49	2.99	
30s	0.1	0.4	20.7		0	0			0			
60s	0.1	0.4	20.7		0	0			0			
90s									0			
120s									0			
150s									0			
180s									0			
210s												
240s												
270s												
300s												

Gas Read Borel		20	05	Surface level (mAOD)				Comm	ents			
Time	CH₄ %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.1	0.2	20.8		0	0	992	-0.02	0	0.66	2.08	
30s	0.1	0.3	20.8		0	0			0.2			
60s	0.1	0.3	20.8		0	0			0.2			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Date	11/02/2014	Weather	Overcast and cold	with falling pressure
Engineer	DM	Atmospheric	Pressure	983
One Boardings at	0	e level		, T



Gas Read Borel		20	)2		e level OD)	2	2.23	Comm	ents			
Time	CH₄ %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.2	0.2	21.1		0	0	983	0.1	0	0.85	1.6	21.38
30s	0.2	0.3	21.1		0	0			0.1			
60s	0.2	0.2	21.1		0	0			0.2			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Gas Read Borel		20	04		e level OD)	2	2.01	Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H₂S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.2	0.2	20.6		0	0	982	-0.19	0	0.42	2.99	21.59
30s	0.2	0.5	20.5		0	0			0			
60s	0.2	0.4	20.5		0	0			0			
90s									0			
120s									0			
150s									0			
180s									0			
210s												
240s												
270s												
300s												

Gas Read Borel		20	05		e level OD)	2	2.12	Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.2	0.2	20.7		0	0	983	-0.03	0	0.65	2.09	21.47
30s	0.2	0.3	20.7		0	1			0.2			
60s	0.2	0.4	20.7		0	1			0.2			
90s									0.2			
120s									0.3			
150s									0.3			
180s									0.3			
210s												
240s												
270s												
300s												

Date	18/02/2014	Weather	Light rain with	level pressure
Engineer	DM	Atmospheric	Pressure	1003



Gas Read Borel		20	02		e level OD)	2	2.23	Comm	ents			
Time	CH₄ %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H₂S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.1	21.3		0	0	1003	-0.26	0	0.85	2.45	21.38
30s	0.0	0.1	21.3		0	0			0.2			
60s	0.0	0.1	21.3		0	0			0.2			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Gas Read Borel		20	04		e level OD)	2	2.01	Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.1	21.3		0	0	1002	0.03	0	0.39	2.99	21.62
30s	0.0	0.1	21.3		0	0			-0.1			
60s	0.0	0.1	21.3		0	0			-0.1			
90s									-0.1			
120s									-0.1			
150s									-0.1			
180s									-0.1			
210s												
240s												
270s												
300s												

Gas Read Borel		20	05		e level OD)	2	2.12	Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.0	0.1	21.2		0	0	1003	-0.19	0	0.61	2.09	21.51
30s	0.0	0.1	21.2		0	0			0.1			
60s	0.0	0.1	21.2		0	0			0.2			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Date	26/02/2014	Weather	Sunny, cool	, light breeze
Engineer	GP	Atmospheric	Pressure	1001-1002



Gas Read Borel		20	)2		e level OD)	2	2.23	Comm	ents			
Time	CH₄ %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H₂S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.2	0.2	21.3		0	0	1001	0.19	0.2	0.84	1.6	21.39
30s	0.2	0.2	21.3		0	0			0.2			
60s	0.1	0.2	21.3		0	0			0.2			
90s									0.1			
120s									0.1			
150s									0.1			
180s									0.1			
210s												
240s												
270s												
300s												

Gas Read Borel		20	04	Surfac (mA		2	2.01	Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.1	0.2	21.2		0	0	1002	0.15	0	0.47	2.99	21.54
30s	0.1	0.2	21.2		0	0			0.1			
60s	0.1	0.2	21.2		0	0			0.2			
90s									0.2			
120s									0.2			
150s									0.2			
180s									0.2			
210s												
240s												
270s												
300s												

Gas Read Borel		20	)5	Surfac (mA	e level OD)	2	2.12	Comm	ents			
Time	CH <sub>4</sub> %vol	CO <sub>2</sub> % vol	O <sub>2</sub> % vol	N <sub>2</sub> % vol	H <sub>2</sub> S ppm	CO ppm	Atmos Pressure (mb)	Diff Pressure (Pa)	Ave Flow (I/h)	G/water Depth (m)	Depth of BH (m)	Water Level (mAOD)
Initial	0.2	0.2	21.2		0	0	1002	0.17	0	0.68	2.08	21.44
30s	0.1	0.2	21.2		0	0			0.1			
60s	0.1	0.2	21.2		0	0			0.1			
90s									0.1			
120s									0.1			
150s									0.1			
180s									0.1			
210s												
240s												
270s												
300s												

# **Modified Wilson and Card Classification** and Typical Scope of Protective Measures

Characteristic	Risk	Gas		esidential Building	Office /	commercial / industrial
Situation	Classification	Screening Value	(not low	rise traditional Housing)		Development
(CIRIA R149)		(CH <sub>4</sub> or CO <sub>2</sub> ) (I/hr)	Levels of Protection	Typical Scope of Protective Measures	Levels of Protection	Typical Scope of Protective Measures
1	Very low	<0.07	None	No special precautions	None	No special precautions
2	Low	<0.7	2	a)Reinforced concrete cast in situ floor slab (suspended, non-suspended or raft) with at least 1200 gauge damp proof membrane and under-floor venting  b)Beam and block or pre-cast concrete and 2000 gauge damp proof membrane/reinforced gas membrane and under-floor venting  All joints and penetrations sealed.	1 to 2	a)Reinforced concrete cast in situ floor slab (suspended, non-suspended or raft) with at least 1200 gauge damp proof membrane and under-floor venting b)Beam and block or pre-cast concrete and 2000 gauge damp proof membrane / reinforced gas membrane and under-floor venting c)Possibly under-floor venting or pressurisation in combination with a) and b) depending on use All joints and penetrations sealed.
3	Moderate	<3.5	2	All types of floor slab as above. All joints and penetrations sealed. Proprietary gas resistant membrane and passively ventilated or positively pressurised under-floor sub- space.	1 to 2	All types of floor slab as above. All joints and penetrations sealed. Minimum 2000g reinforced gas proof membrane and passively vented under-floor sub-space or positively pressurised under-floor sub-space.
4	Moderate to High	<15	3	All types of floor slab as above. All joints and penetrations sealed. Proprietary gas resistant membrane and passively ventilated under-floor subspace or positively pressurised under- floor sub-space, over-site capping or blinding and in ground venting layer.	2 to 3	All types of floor slab as above. All joints and penetrations sealed. Proprietary gas resistant membrane and passively vented under-floor sub-space with monitoring facility.
5	High	<70	4	Reinforced concrete cast in-situ floor slab (suspended, non-suspended or raft). All joints and penetrations sealed. Proprietary gas resistant membrane and ventilated or positively pressurised under-floor subspace, over-site capping and in ground venting layer and in ground venting wells or barriers	3 to 4	Reinforced concrete cast in-situ floor slab (suspended, non-suspended or raft). All joints and penetrations sealed. Proprietary gas resistant membrane and ventilated or positively pressurised under-floor sub-space with monitoring facility. In ground venting wells or barriers.
6	Very High	>70	5	Not suitable unless gas regime is reduced first and quantitative risk assessment carried out to assess design of protection measures in conjunction with foundation design.	4 to 5	Reinforced concrete cast in-situ floor slab (suspended, non-suspended or raft). All joints and penetrations sealed. Proprietary gas resistant membrane and ventilated or positively pressurised under-floor sub-space with monitoring facility. In ground venting wells and reduction of gas regime.

#### Notes:

This table has been reproduced as a combination of data tabulated in CIRIA C665, without the relevant notes and references.

Reference to the full details and guidance notes within CIRIA C665 should be made for further information or in the event of designing gas protection measures.

This table should be used for general guidance only.





**Depot Road** Newmarket CB8 0AL Tel: 01638 606070

Johnson Poole & Bloomer Ltd Harris and Pearson Building **Brettell Lane** Brierly Hill, West Midlands DY5 3LH

**FAO F Townley** 24 January 2014

Dear F Townley

**Test Report Number** 248954

**Your Project Reference NB503 Edhill Avenue** 

Please find enclosed the results of analysis for the samples received 16 January 2014.

All soil samples will be retained for a period of one month and all water samples will be retained for 7 days following the date of the test report. Should you require an extended retention period then please detail your requirements in an email to customerservices@chemtest.co.uk. Please be aware that charges may be applicable for extended sample storage.

If you require any further assistance, please do not hesitate to contact the Customer Services team.

Yours sincerely







Notes to accompany report:

- The sign < means 'less than'
- Tests marked 'U' hold UKAS accreditation
- Tests marked 'M' hold MCertS (and UKAS) accreditation
- Tests marked 'N' do not currently hold UKAS accreditation
- Tests marked 'S' were subcontracted to an approved laboratory
- n/e means 'not evaluated'
- i/s means 'insufficient sample
- u/s means 'unsuitable sample'
- Comments or interpretations are outside of the scope of UKAS accreditation The results relate only to the items tested
- Stones represent the quantity of material removed prior to analysis
- All results are expressed on a dry weight basis
- The following tests were analysed on samples as received and the results subsequently corrected

to a dry weight basis TPH, BTEX, VOCs, SVOCs, PCBs, phenols

- For all other tests the samples were dried at < 37°C prior to analysis
- Uncertainties of measurement for the determinands tested are available upon request Soil descriptions, including colour and texture, are beyond the scope of MCertS accreditation
- None of the test results included in this report have been recovery corrected

**Test Report** 248954 Cover Sheet

FAO F Townley

# LABORATORY TEST REPORT

Chemtest
The right chemistry to deliver results

Report Date 24 January 2014

Results of analysis of 4 samples received 16 January 2014

Login E	Batch No					248	954	
Chemte	est LIMS ID				AJ68913	AJ68914	AJ68915	AJ68917
Sample	: ID				201	205	204	203
Sample	• No							
Samplii	ng Date				9/1/2014	9/1/2014	9/1/2014	9/1/2014
Depth					0.70m	0.10m	0.40m	1.10m
Matrix					SOIL	SOIL	SOIL	SOIL
SOP↓	Determinand↓	CAS No↓ U	nits↓ *					
2030	Moisture		%	M	16.8	15.2	21.1	13.7
	Stones content (>50mm)		%	М	<0.02	<0.02	<0.02	<0.02
2040	Soil colour			М	brown	brown	brown	brown
	Soil texture			М	clay	clay	clay	clay
	Other material			М	stones	stones	stones	stones
2010	pH			М	8.2	8.0	7.3	8.3
2300	Cyanide (free)	57125	mg kg-1	М	<0.50	<0.50	<0.50	<0.50
	Cyanide (total)	57125	mg kg-1	М	<0.50	<0.50	<0.50	<0.50
2625	Total Organic Carbon		%	М	0.90	0.69	5.9	0.56
2120	Boron (hot water soluble)	7440428	mg kg-1	М	1.0	0.8	<0.4	<0.4
	Sulfate (2:1 water soluble) as SO4	14808798	g l-¹	M	0.02	0.02	<0.01	0.02
2490	Chromium (hexavalent)	18540299	mg kg-1	N	<0.5	<0.5	<0.5	<0.5
2450	Arsenic	7440382	mg kg-1	M	6.0	3.6	20	8.6
	Barium	7440393	mg kg-1	M	280	270	240	690
	Beryllium	7440417	mg kg-1	M	1.3	1.1	1.5	1.4
	Cadmium	7440439	mg kg-1	M	<0.10	<0.10	0.36	0.13
	Chromium	7440473	mg kg-1	M	35	31	28	41
	Copper	7440508	mg kg-1	M	28	20	73	29
	Mercury	7439976	mg kg-1	M	<0.10	<0.10	0.39	<0.10
	Nickel	7440020	mg kg-1	M	43	44	25	47
	Lead	7439921	mg kg-1	М	32	16	150	34
	Selenium	7782492	mg kg-1	M	<0.20	<0.20	<0.20	<0.20
	Vanadium	7440622	mg kg-1	M	37	30	73	43
	Zinc	7440666	mg kg-1	M	59	41	130	63

All tests undertaken between 16/01/2014 and 24/01/2014

<sup>\*</sup> Accreditation status

FAO F Townley

## LABORATORY TEST REPORT

Chemtest
The right chemistry to deliver results

Report Date 24 January 2014

Results of analysis of 4 samples received 16 January 2014

				248954			
				AJ68913	AJ68914	AJ68915	AJ68917
				201	205	204	203
				9/1/2014	9/1/2014	9/1/2014	9/1/2014
				0.70m	0.10m	0.40m	1.10m
				SOIL	SOIL	SOIL	SOIL
2675 TPH aliphatic >C5-C6		mg kg-1	N	< 0.1	< 0.1	< 0.1	< 0.1
TPH aliphatic >C6-C8		mg kg-1	N	< 0.1	< 0.1	< 0.1	< 0.1
TPH aliphatic >C8-C10		mg kg-1	N	< 0.1	< 0.1	< 0.1	< 0.1
TPH aliphatic >C10-C12		mg kg-1	М	< 1	< 1	< 1	< 1
TPH aliphatic >C12-C16		mg kg-1	М	< 1	< 1	< 1	< 1
TPH aliphatic >C16-C21		mg kg-1	М	< 1	< 1	< 1	< 1
TPH aliphatic >C21-C35		mg kg-1	М	< 1	< 1	< 1	< 1
TPH aliphatic >C35-C44		mg kg-1	N	< 1	< 1	< 1	< 1
TPH aromatic >C5-C7		mg kg-1	N	< 0.1	< 0.1	< 0.1	< 0.1
TPH aromatic >C7-C8		mg kg-1	N	< 0.1	< 0.1	< 0.1	< 0.1
TPH aromatic >C8-C10		mg kg-1	N	< 0.1	< 0.1	< 0.1	< 0.1
TPH aromatic >C10-C12		mg kg-1	N	< 1	< 1	< 1	< 1
TPH aromatic >C12-C16		mg kg-1	М	< 1	< 1	< 1	< 1
TPH aromatic >C16-C21		mg kg-1	М	< 1	< 1	3.5	< 1
TPH aromatic >C21-C35		mg kg-1	N	< 1	< 1	8.0	< 1
TPH aromatic >C35-C44		mg kg-1	N	< 1	< 1	< 1	< 1
Total Petroleum Hydrocarbons		mg kg-1	N	< 10	< 10	12	< 10
700 Naphthalene	91203	mg kg-1	M	< 0.1	< 0.1	0.68	< 0.1
Acenaphthylene	208968	mg kg-1	M	< 0.1	< 0.1	0.5	< 0.1
Acenaphthene	83329	mg kg-1	M	< 0.1	< 0.1	0.19	< 0.1
Fluorene	86737	mg kg-1	М	< 0.1	< 0.1	0.13	< 0.1
Phenanthrene	85018	mg kg-1	M	< 0.1	< 0.1	0.68	< 0.1
Anthracene	120127	mg kg-1	M	< 0.1	< 0.1	0.26	< 0.1
Fluoranthene	206440	mg kg-1	M	< 0.1	< 0.1	0.75	< 0.1
Pyrene	129000	mg kg-1	M	< 0.1	< 0.1	0.56	< 0.1

All tests undertaken between 16/01/2014 and 24/01/2014

FAO F Townley

# LABORATORY TEST REPORT

Chemtest
The right chemistry to deliver results

Report Date 24 January 2014

Results of analysis of 4 samples received 16 January 2014

						248	954	
					AJ68913	AJ68914	AJ68915	AJ68917
					201	205	204	203
					9/1/2014	9/1/2014	9/1/2014	9/1/2014
					0.70m	0.10m	0.40m	1.10m
					SOIL	SOIL	SOIL	SOIL
2700	Benzo[a]anthracene	56553	mg kg-1	M	< 0.1	< 0.1	0.32	< 0.1
	Chrysene	218019	mg kg-1	М	< 0.1	< 0.1	0.43	< 0.1
	Benzo[b]fluoranthene	205992	mg kg-1	N	< 0.1	< 0.1	0.58	< 0.1
	Benzo[k]fluoranthene	207089	mg kg-1	N	< 0.1	< 0.1	0.26	< 0.1
	Benzo[a]pyrene	50328	mg kg-1	М	< 0.1	< 0.1	0.3	< 0.1
	Dibenzo[a,h]anthracene	53703	mg kg-1	М	< 0.1	< 0.1	< 0.1	< 0.1
	Indeno[1,2,3-cd]pyrene	193395	mg kg-1	М	< 0.1	< 0.1	0.27	< 0.1
	Benzo[g,h,i]perylene	191242	mg kg-1	М	< 0.1	< 0.1	0.29	< 0.1
	Total (of 16) PAHs		mg kg-1	М	< 2	< 2	6.2	< 2
2760	Methyl tert-butylether	1634044	μg kg-¹	М	< 1.0	< 1.0	< 1.0	< 1.0
	Benzene	71432	μg kg-¹	М	< 1.0	< 1.0	< 1.0	< 1.0
	Toluene	108883	μg kg-¹	М	< 1.0	< 1.0	< 1.0	< 1.0
	Ethylbenzene	100414	µg kg-¹	М	< 1.0	< 1.0	< 1.0	< 1.0
	m- & p-Xylene	1330207	µg kg-¹	М	< 1.0	< 1.0	< 1.0	< 1.0
	o-Xylene	95476	µg kg-¹	М	< 1.0	< 1.0	< 1.0	< 1.0
2810	PCB 77	32598133	mg kg-1	N			<0.010	
	PCB 81	70362504	mg kg-1	N			<0.010	
	PCB 105	32598144	mg kg-1	N			<0.010	
	PCB 114	74472370	mg kg-1	N			<0.010	
	PCB 118	31508006	mg kg-1	N			<0.010	
	PCB 123	65510443	mg kg-1	N			<0.010	
	PCB 126	57465288	mg kg-1	N			<0.010	
	PCB 156	38380084	mg kg-1	N			<0.010	
	PCB 157	69782907	mg kg-1	N			<0.010	
	PCB 167	52663726	mg kg-1	N			<0.010	

All tests undertaken between 16/01/2014 and 24/01/2014

FAO F Townley

## LABORATORY TEST REPORT

Chemtest
The right chemistry to deliver results

Results of analysis of 4 samples received 16 January 2014

Report Date 24 January 2014

					248954				
					AJ68913	AJ68914	AJ68915	AJ68917	
					201	205	204	203	
					9/1/2014	9/1/2014	9/1/2014	9/1/2014	
					0.70m	0.10m	0.40m	1.10m	
					SOIL	SOIL	SOIL	SOIL	
2010	DCD 160	22774400	ma ka 1	N			-0.010		
2810	PCB 169	32774166	mg kg-1	N			<0.010		
	PCB 189	39635319	mg kg-1	N			<0.010		
2815	PCB 101	37680732	mg kg-1	M			< 0.01		
	PCB 118	31508006	mg kg-1	М			< 0.01		
	PCB 138	35065282	mg kg-1	M			< 0.01		
	PCB 153	35065271	mg kg-1	М			< 0.01		
	PCB 180	35065293	mg kg-1	M			< 0.01		
	PCB 28	7012375	mg kg-1	M			< 0.01		
	PCB 52	35693993	mg kg-1	М			< 0.01		
2920	Phenols (total)		mg kg-1	M	<0.3	<0.3	<0.3	<0.3	



Depot Road Newmarket CB8 0AL Tel: 01638 606070

Johnson Poole & Bloomer Ltd Harris and Pearson Building Brettell Lane Brierly Hill, West Midlands DY5 3LH

FAO F Townley 24 January 2014

Dear F Townley

Test Report Number 248954

Your Project Reference NB503 Edhill Avenue

Please find enclosed the results of analysis for the samples received 16 January 2014.

If you require any further assistance, please do not hesitate to contact the Customer Services team.

Yours sincerely

Keith Jones, Technical Manager

U KAS TESTING

2193

Notes to accompany report:

- The in-house procedure is employed to identify materials and fibres in soils
- The sample is examined by stereo-binocular and polarised light microscopy
- · Sample size is reduced by coning and quartering to obtain a representative sub-sample if necessary
- The bulk identification is in accordance with the requirements of the analyst guide (HSG 248)
- · Samples associated with asbestos are retained for six months
- The results relate only to the items tested as supplied by the client
- Comments or interpretations are beyond the scope of UKAS accreditation

# LABORATORY TEST REPORT Asbestos in Soils



Results of analysis of 2 samples received 16 January 2014
NB503 Edhill Avenue

Report Date 24 January 2014

FAO F Townley

Login Batch No: 248954

**Qualitative Results** 

				SOP 2190				
				ACM Type	Asbestos Identification			
Chemtest ID	Sample ID	Sample Desc	Depth (m)	UKAS Accredited	UKAS Accredited			
AJ68911	202		0.20	-	No Asbestos Detected			
AJ68914	205		0.10	-	No Asbestos Detected			

The detection limit for this method is 0.001%

Signed

**Albert Vella** 

Senior Environmental Surveyor



**Depot Road** Newmarket CB8 0AL Tel: 01638 606070

Johnson Poole & Bloomer Ltd Harris and Pearson Building **Brettell Lane** Brierly Hill, West Midlands DY5 3LH

**FAO F Townley** 04 February 2014

Dear F Townley

**Test Report Number** 249877

**Your Project Reference NB503 Edhill Avenue** 

Please find enclosed the results of analysis for the samples received 27 January 2014.

All soil samples will be retained for a period of one month and all water samples will be retained for 7 days following the date of the test report. Should you require an extended retention period then please detail your requirements in an email to customerservices@chemtest.co.uk. Please be aware that charges may be applicable for extended sample storage.

If you require any further assistance, please do not hesitate to contact the Customer Services team.

Yours sincerely





- Notes to accompany report:
- The sign < means 'less than'
- Tests marked 'U' hold UKAS accreditation
- Tests marked 'M' hold MCertS (and UKAS) accreditation Tests marked 'N' do not currently hold UKAS accreditation
- Tests marked 'S' were subcontracted to an approved laboratory
- n/e means 'not evaluated'
- i/s means 'insufficient sample
- u/s means 'unsuitable sample'
- Comments or interpretations are beyond the scope of UKAS accreditation
- The results relate only to the items tested
- All results are expressed on a dry weight basis
- The following tests were analysed on samples as received and the results subsequently corrected to a dry weight basis TPH, BTEX, VOCs, SVOCs, PCBs, phenols
- For all other tests the samples were dried at < 37°C prior to analysis
- Uncertainties of measurement for the determinands tested are available upon request
- None of the test results included in this report have been recovery corrected

**Test Report** 249877 Cover Sheet

FAO F Townley

# LABORATORY TEST REPORT

Chemtest
The right chemistry to deliver results

Results of analysis of 1 sample received 27 January 2014

Report Date 04 February 2014

Login E	Batch No				249877
Chemte	est LIMS ID				AJ74507
Sample	ID				202
Sample	· No				
Sampli	ng Date				21/1/2014
Depth					
Matrix					WATER
SOP↓	Determinand↓	CAS No↓ L	Inits↓ *		
1010	рН	PH		U	7.8
1020	Electrical Conductivity	EC	μS cm-1	U	850
1300	Cyanide (total)	57125	mg l-1	U	< 0.050
	Cyanide (free)	57125	mg l-1	U	< 0.050
1220	Alkalinity	ALK	mg CaCO3 I-1	U	330
1325	Sulfide	18496258	mg l-1	U	< 0.050
1610	Total Organic Carbon	TOC	mg l-1	N	4.1
1220	Sulfate	14808798	mg l-1	U	120
1450	Arsenic	7440382	μg l-¹	U	1.2
	Boron	7440428	μg l-¹	U	32
	Barium	7440393	μg l-¹	U	75
	Beryllium	7440417	μg l-¹	U	<1.0
	Cadmium	7440439	μg l-¹	U	<0.080
	Chromium	7440473	μg l-¹	U	<1.0
	Copper	7440508	μg l-¹	U	2.3
	Mercury	7439976	μg l-¹	U	< 0.50
	Nickel	7440020	μg l-¹	U	<1.0
	Lead	7439921	μg l-¹	U	<1.0
	Selenium	7782492	μg l-¹	U	8.4
	Vanadium	7440622	μg l-¹	U	<1.0
	Zinc	7440666	μg l-¹	U	5.3
1490	Chromium (hexavalent)	18540299	μg l-¹	U	<20
1675	TPH aliphatic >C5-C6		μg l-¹	N	< 0.1
	TPH aliphatic >C6-C8		μg l-¹	N	< 0.1

FAO F Townley

## LABORATORY TEST REPORT

Chemtest
The right chemistry to deliver results

Results of analysis of 1 sample received 27 January 2014

Report Date 04 February 2014

					249877
					AJ74507
					202
					21/1/2014
					WATER
1675	TPH aliphatic >C8-C10		μg l-¹	N	< 0.1
	TPH aliphatic >C10-C12		μg l-¹	N	< 0.1
	TPH aliphatic >C12-C16		µg l-¹	N	< 0.1
	TPH aliphatic >C16-C21		µg l-¹	N	< 0.1
	TPH aliphatic >C21-C35		μg l-¹	N	< 0.1
	TPH aliphatic >C35-C44		μg l-¹	N	< 0.1
	TPH aromatic >C5-C7		µg l-¹	N	< 0.1
	TPH aromatic >C7-C8		µg l-¹	N	< 0.1
	TPH aromatic >C8-C10		µg l-¹	N	< 0.1
	TPH aromatic >C10-C12		μg l-¹	N	< 0.1
	TPH aromatic >C12-C16		μg l-¹	N	< 0.1
	TPH aromatic >C16-C21		μg l-¹	N	< 0.1
	TPH aromatic >C21-C35		μg l-¹	N	< 0.1
	TPH aromatic >C35-C44		μg l-¹	N	< 0.1
	Total Petroleum Hydrocarbons		μg l−¹	N	< 10
	Total Aliphatic Hydrocarbons		µg l−¹	N	< 5
	Total Aromatic Hydrocarbons		μg l−¹	N	< 5
1700	Naphthalene	91203	µg l−¹	U	<0.1
	Acenaphthylene	208968	μg I-1	U	<0.1
	Acenaphthene	83329	μg I-1	U	<0.1
	Fluorene	86737	μg l-1	U	<0.1
	Phenanthrene	85018	μg l-1	U	<0.1
	Anthracene	120127	μg l-1	U	<0.1
	Fluoranthene	206440	μg l-1	U	<0.1
	Pyrene	129000	μg l-1	U	<0.1

All tests undertaken between 27/01/2014 and 04/02/2014

FAO F Townley

# LABORATORY TEST REPORT

Chemtest
The right chemistry to deliver results

Report Date
04 February 2014

Results of analysis of 1 sample received 27 January 2014

				249877
				AJ74507
				202
				21/1/2014
				WATER
1700 Benzo[a]anthracene	56553	μg l-¹	U	<0.1
Chrysene	218019	μg l-¹	U	<0.1
Benzo[b]fluoranthene	205992	μg l-¹	N	<0.1
Benzo[k]fluoranthene	207089	μg l-¹	N	<0.1
Benzo[a]pyrene	50328	μg l-¹	U	<0.1
Dibenzo[a,h]anthracene	53703	μg l-¹	U	<0.1
Indeno[1,2,3-cd]pyrene	193395	μg l-¹	U	<0.1
Benzo[g,h,i]perylene	191242	μg l-¹	U	<0.1
Total (of 16) PAHs		μg l-¹	U	<2
1760 Methyl tert-butylether	1634044	μg l-¹	N	<1.0
Benzene	71432	μg l-¹	U	<1.0
Toluene	108883	μg l-¹	U	<1.0
Ethylbenzene	100414	μg l-¹	U	<1.0
m- & p-Xylene	1330207	μg l-¹	U	<1.0
o-Xylene	95476	μg l-¹	U	<1.0
1815 PCB 101	37680732	μg l-¹	N	<0.010
PCB 105	32598144	μg l-¹	N	<0.010
PCB 114	74472370	μg l-¹	N	<0.010
PCB 118	31508006	μg l-¹	N	<0.010
PCB 123	65510443	μg l-¹	N	<0.010
PCB 126	57465288	μg l-¹	N	<0.010
PCB 138	35065282	μg l-¹	N	<0.010
PCB 153	35065271	μg l-¹	N	<0.010
PCB 156	38380084	μg l-¹	N	<0.010
PCB 157	69782907	μg l-¹	N	<0.010

All tests undertaken between 27/01/2014 and 04/02/2014

Johnson Poole & Bloomer Ltd Harris and Pearson Building Brettell Lane Brierly Hill, West Midlands DY5 3LH

FAO F Townley

# LABORATORY TEST REPORT

Chemtest
The right chemistry to deliver results

Report Date 04 February 2014

Results of analysis of 1 sample received 27 January 2014

**NB503 Edhill Avenue** 

					249877
					AJ74507
					202
					21/1/2014
					WATER
1815	PCB 167	52663726	μg l-¹	N	<0.010
	PCB 169	32774166	μg l-¹	N	<0.010
	PCB 180	35065293	μg l-¹	N	<0.010
	PCB 189	39635319	μg l-¹	N	<0.010
	PCB 28	7012375	μg l-¹	N	<0.010
	PCB 52	35693993	μg l-¹	N	<0.010
	PCB 77	32598133	μg l-¹	N	<0.010
	PCB 81	70362504	μg l-¹	N	<0.010
1920	Phenols (total)		mg l-1	N	< 0.03



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Environment Agency

Report generated

30-Jan-14

Report title

Edhill Avenue Residential with Plant Uptake

Created by

FT at JPB

RESULTS

Report generated 30-Jan-14

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		Assessm	ent Criterion	(mg kg <sup>-1</sup> )	Ratio	o of ADE to	HCV	Continuation Limits (see Levil)	50%	rule?
		oral	inhalation	combined	oral	inhalation	combined	Saturation Limit (mg kg <sup>-1</sup> )	Oral	Inhal
1	Boron JPB	2.91E+02	1.22E+05	2.91E+02	1.00	0.00	1.00	NR	Yes	No
2	Arsenic	3.24E+01	8.50E+01	NR	1.00	0.38	NR	NR	No	No
3	Barium	1.33E+03	NR	NR	1.00	NR	NR	NR	Yes	No
4	Chromium (III) JPB	1.95E+04	6.37E+02	6.27E+02	0.03	0.97	1.00	NR	No	Yes
5	Copper JPB	2.66E+03	1.04E+04	2.33E+03	0.78	0.22	1.00	NR	Yes	No
6	Mercury, inorganic	1.81E+02	2.55E+03	1.69E+02	0.93	0.07	1.00	NR	No	No
7	Nickel	5.31E+02	1.27E+02	NR	0.14	1.00	NR	NR	Yes	Yes
8	Vanadium JPB	7.96E+01	6.08E+02	7.44E+01	0.93	0.07	1.00	NR	Yes	Yes
9	Zinc JPB	3.75E+03	2.55E+07	3.75E+03	1.00	0.00	1.00	NR	Yes	No
10	Aromatic >EC16 - EC21 JPB	2.41E+02	NR	NR	1.00	NR	NR	5.17E+01 (vap)	Yes	No
11	Aromatic >EC21 - EC35 JPB	8.77E+02	NR	NR	1.00	NR	NR	4.64E+00 (sol)	Yes	No
12	Naphthalene JPB	2.68E+01	4.98E+00	4.20E+00	0.16	0.84	1.00	7.86E+01 (sol)	No	No
13	Acenaphthylene JPB	1.73E+02	3.09E+03	1.64E+02	0.95	0.05	1.00	8.49E+01 (sol)	No	No
14	Acenaphthene JPB	2.12E+02	3.50E+03	2.00E+02	0.94	0.06	1.00	5.59E+01 (sol)	No	No
15	Fluorene JPB	1.65E+02	3.82E+03	1.58E+02	0.96	0.04	1.00	3.02E+01 (sol)	No	No
16	Phenanthrene JPB	9.05E+01	4.52E+03	8.87E+01	0.98	0.02	1.00	3.49E+01 (sol)	No	No
17	Anthracene JPB	2.23E+03	9.37E+04	2.18E+03	0.98	0.02	1.00	1.13E+00 (vap)	No	No
18	Fluoranthene JPB	2.52E+02	2.76E+04	2.49E+02	0.99	0.01	1.00	1.82E+01 (vap)	No	No
19	Pyrene JPB	5.52E+02	6.50E+04	5.47E+02	0.99	0.01	1.00	2.12E+00 (vap)	No	No
20	Benz[a]anthracene JPB	6.89E+00	6.13E+00	3.25E+00	0.47	0.53	1.00	1.64E+00 (sol)	No	No

Report generated 30-Jan-14

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		Assessn	nent Criterion	(mg kg <sup>-1</sup> )	Ratio	o of ADE to I	HCV	a	50%	rule?
		oral	inhalation	combined	oral	inhalation	combined	Saturation Limit (mg kg <sup>-1</sup> )	Oral	Inhal
21	Chrysene JPB	8.51E+00	2.08E+01	6.04E+00	0.71	0.29	1.00	4.23E-01 (vap)	No	No
22	Benzo[b]fluoranthene JPB	7.96E+00	1.80E+01	5.53E+00	0.69	0.31	1.00	1.17E+00 (sol)	No	No
23	Benzo[k]fluoranthene JPB	1.24E+01	2.66E+01	8.45E+00	0.68	0.32	1.00	6.59E-01 (sol)	No	No
24	Benzo[a]pyrene JPB	1.19E+00	2.62E+00	8.20E-01	0.69	0.31	1.00	8.75E-01 (vap)	No	No
25	Indeno[123-cd]pyrene JPB	4.52E+00	1.06E+01	3.17E+00	0.70	0.30	1.00	5.90E-02 (vap)	No	No
26	Benzo[ghi]perylene JPB	6.65E+01	1.28E+02	4.38E+01	0.66	0.34	1.00	1.48E-02 (vap)	No	No
27	Beryllium JPB	1.12E+02	5.10E+01	3.84E+01	0.25	0.75	1.00	NR	Yes	No
28										
29		] 								
30									[	

# CLEA Software Version 1.06 Report generated 30-Jan-14 Page 4 of 11

6	Environment Agency	5	Soil Dist	ributio	n							Media	a Concentr	ations					
		Sorbed	Dissolved	Vapour	Total	Soil	Soil gas	Indoor Dust	Outdoor dust at 0.8m	Outdoor dust at 1.6m	Indoor Vapour	Outdoor vapour at 0.8m	Outdoor vapour at 1.6m	Green vegetables	Root vegetables	Tuber vegetables	Herbaceous fruit	Shrub fruit	Tree fruit
		%	%	%	%	mg kg <sup>-1</sup>	mg m <sup>-3</sup>	mg kg <sup>-1</sup>	mg m⁻³	mg m⁻³	mg m⁻³	mg m <sup>-3</sup>	mg m⁻³	mg kg <sup>-1</sup> FW	i	mg kg <sup>-1</sup> FW			
1	Boron JPB	94.6	5.4	0.0	100.0	2.91E+02	NR	1.46E+02	1.24E-07	0.00E+00	0.00E+00	0.00E+00	0.00E+00	1.16E+02	5.82E+01	5.82E+01	5.82E+01	5.82E+01	5.82E+01
2	Arsenic	99.9	0.1	0.0	100.0	3.24E+01	NR	1.62E+01	1.38E-08	0.00E+00	0.00E+00	0.00E+00	0.00E+00	1.39E-02	1.30E-02	7.45E-03	1.07E-02	6.48E-03	3.56E-02
3	Barium	#DIV/0!	#DIV/0!	0.0	#DIV/0!	1.33E+03	NR	6.64E+02	5.66E-07	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
4	Chromium (III) JPB	100.0	0.0	0.0	100.0	6.27E+02	NR	3.14E+02	2.67E-07	0.00E+00	0.00E+00	0.00E+00	0.00E+00	1.88E-02	1.88E-02	1.88E-02	1.88E-02	1.88E-02	1.88E-02
5	Copper JPB	99.5	0.5	0.0	100.0	2.33E+03	NR	1.16E+03	9.90E-07	0.00E+00	0.00E+00	0.00E+00	0.00E+00	4.79E+01	4.79E+01	4.79E+01	5.42E+01	4.79E+01	4.79E+01
6	Mercury, inorganic	99.9	0.1	0.0	100.0	1.69E+02	NR	8.43E+01	7.18E-08	0.00E+00	0.00E+00	0.00E+00	0.00E+00	6.41E-01	1.16E+00	7.25E-01	1.69E-01	1.86E-01	1.69E-01
7	Nickel	99.9	0.1	0.0	100.0	1.27E+02	NR	6.37E+01	5.42E-08	0.00E+00	0.00E+00	0.00E+00	0.00E+00	4.84E-01	5.48E-01	2.42E-01	3.19E-01	3.19E-01	4.33E-01
8	Vanadium JPB	95.7	4.3	0.0	100.0	7.44E+01	NR	3.72E+01	3.17E-08	0.00E+00	0.00E+00	0.00E+00	0.00E+00	9.67E-01	9.67E-01	9.67E-01	9.67E-01	9.67E-01	9.67E-01
9	Zinc JPB	98.6	1.4	0.0	100.0	3.75E+03	NR	1.87E+03	1.59E-06	0.00E+00	0.00E+00	0.00E+00	0.00E+00	2.02E+02	2.02E+02	2.02E+02	5.36E+02	2.02E+02	2.02E+02
10	Aromatic >EC16 - EC21 JPB	99.3	0.7	0.0	100.0	2.41E+02	2.11E+00	1.20E+02	1.03E-07	0.00E+00	1.08E-04	1.51E-05	0.00E+00	1.84E+01	2.88E+01	1.72E+01	0.00E+00	0.00E+00	9.03E-01
11	Aromatic >EC21 - EC35 JPB	99.9	0.1	0.0	100.0	8.77E+02	3.10E-02	4.39E+02	3.73E-07	0.00E+00	2.64E-06	1.80E-05	0.00E+00	3.17E+00	1.24E+01	1.85E+01	0.00E+00	0.00E+00	2.83E-02
12	Naphthalene JPB	86.9	13.1	0.0	100.0	4.20E+00	6.72E+00	2.10E+00	1.79E-09	0.00E+00	6.29E-04	1.04E-06	0.00E+00	4.14E+00	6.44E+00	1.47E+00	0.00E+00	0.00E+00	1.87E+00
13	Acenaphthylene JPB	94.9	5.1	0.0	100.0	1.64E+02	8.73E+00	8.20E+01	6.98E-08	0.00E+00	3.44E-03	1.94E-05	0.00E+00	8.83E+01	1.23E+02	3.05E+01	0.00E+00	0.00E+00	1.71E+01
14	Acenaphthene JPB	96.0	4.0	0.0	100.0	2.00E+02	1.12E+01	1.00E+02	8.52E-08	0.00E+00	3.71E-03	2.09E-05	0.00E+00	8.83E+01	1.22E+02	3.37E+01	0.00E+00	0.00E+00	1.43E+01
15	Fluorene JPB	96.7	3.3	0.0	100.0	1.58E+02	4.01E+00	7.90E+01	6.72E-08	0.00E+00	1.78E-03	1.45E-05	0.00E+00	6.00E+01	8.30E+01	2.37E+01	0.00E+00	0.00E+00	8.37E+00
16	Phenanthrene JPB	98.3	1.7	0.0	100.0	8.87E+01	4.07E-01	4.43E+01	3.77E-08	0.00E+00	2.62E-04	5.70E-06	0.00E+00	1.82E+01	2.61E+01	9.20E+00	0.00E+00	0.00E+00	1.45E+00
17	Anthracene JPB	98.3	1.7	0.0	100.0	2.18E+03	1.24E+01	1.09E+03	9.28E-07	0.00E+00	7.49E-03	1.39E-04	0.00E+00	4.37E+02	6.26E+02	2.22E+02	0.00E+00	0.00E+00	3.49E+01
18	Fluoranthene JPB	99.5	0.5	0.0	100.0	2.49E+02	1.54E-01	1.25E+02	1.06E-07	0.00E+00	1.15E-04	8.62E-06	0.00E+00	1.29E+01	2.38E+01	1.25E+01	0.00E+00	0.00E+00	3.98E-01
19	Pyrene JPB	99.4	0.6	0.0	100.0	5.47E+02	3.40E-01	2.74E+02	2.33E-07	0.00E+00	2.58E-04	2.01E-05	0.00E+00	3.26E+01	5.83E+01	3.00E+01	0.00E+00	0.00E+00	1.09E+00
20	Benz[a]anthracene JPB	99.9	0.1	0.0	100.0	3.25E+00	2.37E-04	1.62E+00	1.38E-09	0.00E+00	1.90E-07	5.22E-08	0.00E+00	2.00E-02	7.44E-02	5.15E-02	0.00E+00	0.00E+00	1.89E-04

CLEA Software Versio	n 1.0	6				Repo	ort generated			30-Jan-14							Page 5 of 1	1
Environment Agency	5	Soil Dist	tributio	n							Media	Concentra	tions					
	Sorbed	Dissolved	Vapour	Total	Soil	Soil gas	Indoor Dust	Outdoor dust at 0.8m	Outdoor dust at 1.6m	Indoor Vapour	Outdoor vapour at 0.8m	Outdoor vapour at 1.6m	Green vegetables	Root vegetables	Tuber vegetables	Herbaceous fruit	Shrub fruit	Tree fruit
	%	%	%	%	mg kg <sup>-1</sup>	mg m <sup>-3</sup>	mg kg <sup>-1</sup>	mg m <sup>-3</sup>	mg m⁻³	mg m <sup>-3</sup>	mg m <sup>-3</sup>	mg m <sup>-3</sup>	i		mg kg <sup>-1</sup> FW		mg kg <sup>-1</sup> FW	mg kg <sup>-1</sup> FW
21 Chrysene JPB	99.8	0.2	0.0	100.0	6.04E+00	6.27E-05	3.02E+00	2.57E-09	0.00E+00	6.05E-08	1.15E-07	0.00E+00	6.42E-02	1.95E-01	1.27E-01	0.00E+00	0.00E+00	8.00E-04
22 Benzo[b]fluoranthene JPB	99.9	0.1	0.0	100.0	5.53E+00	1.94E-05	2.76E+00	2.35E-09	0.00E+00	2.15E-08	7.46E-08	0.00E+00	2.03E-02	9.41E-02	6.48E-02	0.00E+00	0.00E+00	1.48E-04
23 Benzo[k]fluoranthene JPB	99.9	0.1	0.0	100.0	8.45E+00	1.78E-05	4.23E+00	3.60E-09	0.00E+00	2.14E-08	9.60E-08	0.00E+00	1.71E-02	1.02E-01	7.24E-02	0.00E+00	0.00E+00	9.43E-05
24 Benzo[a]pyrene JPB	99.9	0.1	0.0	100.0	8.20E-01	2.01E-06	4.10E-01	3.49E-10	0.00E+00	2.41E-09	1.00E-08	0.00E+00	2.13E-03	1.14E-02	8.05E-03	0.00E+00	0.00E+00	1.34E-05
25 Indeno[123-cd]pyrene JPB	99.9	0.1	0.0	100.0	3.17E+00	1.34E-05	1.58E+00	1.35E-09	0.00E+00	1.46E-08	4.61E-08	0.00E+00	1.61E-02	6.47E-02	4.24E-02	0.00E+00	0.00E+00	1.39E-04
26 Benzo[ghi]perylene JPB	100.0	0.0	0.0	100.0	4.38E+01	5.40E-05	2.19E+01	1.87E-08	0.00E+00	5.28E-08	2.94E-07	0.00E+00	1.23E-02	1.88E-01	1.38E-01	0.00E+00	0.00E+00	2.80E-05
27 Beryllium JPB	100.0	0.0	0.0	100.0	3.84E+01	NR	1.92E+01	1.63E-08	0.00E+00	0.00E+00	NR	0.00E+00	2.69E-01	4.61E-02	4.61E-02	4.61E-02	4.61E-02	4.61E-02
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E.	Environment Agency		Avera	ge Daily Ex	posure (m	g kg <sup>-1</sup> bw c	lay <sup>-1</sup> )				Distr	ribution by	/ Pathwa	y (%)		
		Direct soil ingestion	Consumption of homegrown produce and attached soil	Dermal contact with soil and dust	Inhalation of dust	Inhalation of vapour	Background (oral)	Background (inhalation)	Direct soil ingestion	Consumption of homegrown produce and attached soil	Dermal contact with soil and dust	Inhalation of dust	Inhalation of vapour (indoor)	Inhalation of vapour (outdoor)	Background (oral)	Background (inhalation)
1	Boron JPB	2.16E-03	7.78E-02	0.00E+00	6.85E-06	0.00E+00	2.08E-01	2.41E-05	1.35	48.65	0.00	0.00	0.00	0.00	50.00	0.00
2	Arsenic	2.40E-04	2.27E-05	3.70E-05	7.62E-07	0.00E+00	0.00E+00	0.00E+00	79.89	7.54	12.31	0.25	0.00	0.00	0.00	0.00
3	Barium	9.86E-03	1.13E-04	0.00E+00	3.13E-05	0.00E+00	4.77E-02	6.06E-02	49.28	0.57	0.00	0.16	0.00	0.00	50.00	0.00
4	Chromium (III) JPB	4.65E-03	7.37E-05	0.00E+00	1.48E-05	0.00E+00	3.39E-03	1.64E-05	57.13	0.91	0.00	0.18	0.00	0.00	41.60	0.18
5	Copper JPB	1.73E-02	5.26E-02	0.00E+00	5.48E-05	0.00E+00	3.94E-01	4.12E-05	12.34	37.63	0.00	0.04	0.00	0.00	49.97	0.03
6	Mercury, inorganic	1.25E-03	5.64E-04	0.00E+00	3.97E-06	0.00E+00	5.63E-05	0.00E+00	66.71	30.08	0.00	0.21	0.00	0.00	3.00	0.00
7	Nickel	9.45E-04	4.66E-04	2.43E-05	3.00E-06	0.00E+00	7.31E-03	3.64E-06	32.77	16.18	0.84	0.10	0.00	0.00	49.90	0.10
8	Vanadium JPB	5.52E-04	1.04E-03	0.00E+00	1.75E-06	0.00E+00	1.29E-03	3.88E-05	19.07	36.07	0.00	0.06	0.00	0.00	44.74	0.06
9	Zinc JPB	2.78E-02	2.72E-01	0.00E+00	8.81E-05	0.00E+00	1.52E+00	1.45E-04	4.63	45.36	0.00	0.01	0.00	0.00	49.99	0.01
10	Aromatic >EC16 - EC21 JPB	1.79E-03	1.23E-02	9.18E-04	5.67E-06	1.00E-04	5.62E+95	0.00E+00	5.96	40.98	3.06	0.00	0.00	0.00	50.00	0.00
11	Aromatic >EC21 - EC35 JPB	6.51E-03	5.15E-03	3.34E-03	2.06E-05	3.19E-06	5.62E+95	0.00E+00	21.69	17.17	11.14	0.00	0.00	0.00	50.00	0.00
12	Naphthalene JPB	3.12E-05	3.02E-03	2.08E-05	9.89E-08	5.82E-04	3.94E-04	1.70E-04	0.74	71.61	0.49	0.00	13.79	0.00	9.34	4.02
13	Acenaphthylene JPB	1.22E-03	5.48E-02	8.12E-04	3.86E-06	3.18E-03	7.88E-06	6.67E-07	2.03	91.29	1.35	0.01	5.31	0.00	0.01	0.00
14	Acenaphthene JPB	1.48E-03	5.40E-02	9.91E-04	4.71E-06	3.43E-03	5.51E-05	1.52E-06	2.47	90.06	1.65	0.01	5.71	0.00	0.09	0.00
15	Fluorene JPB	1.17E-03	3.64E-02	7.83E-04	3.72E-06	1.65E-03	3.32E-05	5.82E-06	2.93	90.89	1.96	0.01	4.12	0.00	0.08	0.01
16	Phenanthrene JPB	6.58E-04	1.11E-02	4.39E-04	2.09E-06	2.43E-04	8.66E-05	3.14E-05	5.25	88.35	3.51	0.02	1.94	0.00	0.69	0.25
17	Anthracene JPB	1.62E-02	2.66E-01	1.08E-02	5.13E-05	6.93E-03	4.50E-06	2.49E-06	5.39	88.68	3.60	0.02	2.31	0.00	0.00	0.00
18	Fluoranthene JPB	1.85E-03	9.28E-03	1.24E-03	5.87E-06	1.07E-04	1.97E-05	5.09E-06	14.80	74.22	9.88	0.05	0.85	0.00	0.16	0.04
19	Pyrene JPB	4.06E-03	2.30E-02	2.71E-03	1.29E-05	2.40E-04	1.97E-05	3.94E-06	13.52	76.52	9.03	0.04	0.80	0.00	0.07	0.01
20	Benz[a]anthracene JPB	2.41E-05	2.48E-05	1.61E-05	7.64E-08	1.78E-07	3.38E-06	6.67E-07	36.90	38.06	24.65	0.12	0.27	0.00	0.00	0.00

#### CLEA Software Version 1.06 Report generated 30-Jan-14 Page 7 of 11 Environment Agency Average Daily Exposure (mg kg<sup>-1</sup> bw day<sup>-1</sup>) Distribution by Pathway (%) Consumption of homegrown produce Dermal contact with soil and dust Dermal contact with soil and dust Direct soil ingestion nhalation of vapour Direct soil ingestion Consumption of homegrown produand attached soil ackground (oral) Background (inhalation) Background (inhalation) 21 Chrysene JPB 4.48E-05 6.73E-05 2.99E-05 1.42E-07 6.07E-08 6.19E-06 1.03E-06 31.50 21.04 0.10 0.04 0.00 0.00 0.00 22 Benzo[b]fluoranthene JPB 4.10E-05 3.02E-05 2.74E-05 1.30E-07 2.30E-08 6.19E-06 7.88E-07 41.53 30.58 27.74 0.13 0.02 0.00 0.00 0.00 23 Benzo[k]fluoranthene JPB 6.27E-05 3.18E-05 4.19E-05 1.99E-07 2.38E-08 5.06E-06 4.24E-07 45.89 23.30 30.65 0.15 0.01 0.00 0.00 0.00 24 Benzo[a]pyrene JPB 6.08E-06 3.59E-06 4.06E-06 1.93E-08 2.65E-09 6.19E-06 3.64E-07 44.19 26.13 29.51 0.14 0.02 0.00 0.00 0.00 25 Indeno[123-cd]pyrene JPB 2.35E-05 2.11E-05 1.57E-05 7.45E-08 1.55E-08 5.63E-06 5.46E-07 38.93 34.91 26.00 0.12 0.02 0.00 0.00 0.00 26 Benzo[ghi]perylene JPB 3.25E-04 5.66E-05 2.17E-04 1.03E-06 6.11E-08 3.38E-06 6.06E-07 54.19 9.43 36.19 0.17 0.01 0.00 0.00 0.00 27 Beryllium JPB 2.85E-04 1.11E-04 0.00E+00 9.04E-07 0.00E+00 8.44E-04 0.00E+00 35.92 14.03 0.00 0.11 0.00 0.00 49.94 0.00 28

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Environment Agency		Oral Health Criteria Value (µg kg¹ BW day¹)		innalation reauth Criteria value (µg kgʻ¹ BW dayʻ¹)	Oral Mean Daily Intake (µg day¹)	Inhalation Mean Daily Intake (µg day <sup>-1</sup> )	Air-water partition coefficient $(K_{aw})$ $(cm^3 cm^3)$	Coefficient of Diffusion in Air $(m^2s^1)$	Coefficient of Diffusion in Water $({\rm m}^2{\rm s}^1)$	$\log K_{\infty}  (cm^3 g^{-1})$	log K <sub>ow</sub> (dimensionless)	Dermal Absorption Fraction (dimensionless)	Soil-to-dust transport factor (g g <sup>-1</sup> DW)	Sub-surface soil to indoor air correction factor (dimensionless)	Relative bioavailability via soil ingestion (unitless)	Relative bioavailability via dust inhalation (unitless)
1 Boron JPB	TDI	160	TDI	2.9	3700	0.398	NR	NR	NR	NR	NR	0	0.5	1	1	1
2 Arsenic	ID	0.3	ID	0.002	NR	NR	NR	NR	NR	NR	NR	0.03	0.5	1	1	1
3 Barium	TDI	20	NR	0	847	1000	NR	NR	NR	NR	NR	0	0.5	1	1	1
4 Chromium (III) JPB	TDI	150	TDI	0.03	60.2	0.27	NR	NR	NR	NR	NR	0	0.5	1	1	1
5 Copper JPB	TDI	160	TDI	0.286	7000	0.68	NR	NR	NR	NR	NR	0	0.5	1	1	1
6 Mercury, inorganic	TDI	2	TDI	0.06	1	0	NR	NR	NR	NR	NR	0	0.5	1	1	1
7 Nickel	TDI	12	TDI	0.006	130	0.06	NR	NR	NR	NR	NR	0.005	0.5	1	1	1
8 Vanadium JPB	TDI	3	TDI	0.0286	23	0.64	NR	NR	NR	NR	NR	0	0.5	1	1	1
9 Zinc JPB	TDI	600	TDI	600	27000	2.4	NR	NR	NR	NR	NR	0	0.5	1	1	1
10 Aromatic >EC16 - EC21 JPB	TDI	30	NR	0	9.99E+99	NR	6.95E-04	1.00E-05	1.00E-09	4.15	4.82	0.1	0.5	10	1	1
11 Aromatic >EC21 - EC35 JPB	TDI	30	NR	0	9.99E+99	NR	2.48E-05	1.00E-05	1.00E-09	5.1	5.95	0.1	0.5	10	1	1
12 Naphthalene JPB	TDI	20	TDI	0.86	7	2.8	6.62E-03	6.52E-06	5.16E-10	2.81	3.34	0.13	0.5	1	1	1
13 Acenaphthylene JPB	TDI	60	TDI	60	0.14	0.011	5.68E-04	5.97E-06	4.82E-10	3.26	3.91	0.13	0.5	1	1	1
14 Acenaphthene JPB	TDI	60	TDI	60	0.98	0.025	7.59E-04	5.85E-06	4.70E-10	3.37	4.03	0.13	0.5	1	1	1
15 Fluorene JPB	TDI	40	TDI	40	0.59	0.096	4.12E-04	5.58E-06	4.47E-10	3.45	4.13	0.13	0.5	1	1	1
16 Phenanthrene JPB	TDI	12.5	TDI	12.5	1.54	0.518	1.43E-04	5.34E-06	4.32E-10	3.74	4.5	0.13	0.5	1	1	1
17 Anthracene JPB	TDI	300	TDI	300	0.08	0.041	1.81E-04	5.36E-06	4.36E-10	3.75	4.5	0.13	0.5	1	1	1
18 Fluoranthene JPB	TDI	12.5	TDI	12.5	0.35	0.084	6.29E-05	5.01E-06	4.11E-10	4.26	5.13	0.13	0.5	1	1	1
19 Pyrene JPB	TDI	30	TDI	30	0.35	0.065	5.64E-05	5.01E-06	4.15E-10	4.21	5.08	0.13	0.5	1	1	1
20 Benz[a]anthracene JPB	ID	0.138	ID	0.00048	0.06	0.011	3.16E-05	4.60E-06	3.80E-10	4.89	5.91	0.13	0.5	1	1	1

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Environment Agency		Oral Health Criteria Value (µg kg¹ BW day¹)		innalation Health Criteria Value (µg kgʻ¹ BW dayʻ¹)	Oral Mean Daily Intake (µg day⁻¹)	Inhalation Mean Daily Intake (µg day <sup>-1</sup> )	Air-water partition coefficient (K <sub>sw.</sub> ) (cm <sup>3</sup> cm <sup>-3</sup> )	Coefficient of Diffusion in Air $(m^2  s^1)$	Coefficient of Diffusion in Water $(m^2 \ s^1)$	$\log K_{\infty} (cm^3 g^{-1})$	log K <sub>ow</sub> (dimensionless)	Dermal Absorption Fraction (dimensionless)	Soil-to-dust transport factor (gg-¹ DW)	Sub-surface soil to indoor air correction factor (dimensionless)	Relative bioavailability via soil ingestion (unitless)	Relative bioavailability via dust inhalation (unitless)
21 Chrysene JPB	ID	0.2	ID	0.0007	0.11	0.017	3.18E-06	4.57E-06	3.77E-10	4.74	5.73	0.13	0.5	1	1	1
22 Benzo[b]fluoranthene JPB	ID	0.142	ID	0.0005	0.11	0.013	2.05E-06	4.38E-06	3.62E-10	5.02	6.08	0.13	0.5	1	1	1
23 Benzo[k]fluoranthene JPB	ID	0.2	ID	0.0007	0.09	0.007	1.74E-06	4.36E-06	3.62E-10	5.17	6.26	0.13	0.5	1	1	1
24 Benzo[a]pyrene JPB	ID	0.02	ID	0.00007	0.11	0.006	1.76E-06	4.38E-06	3.67E-10	5.11	6.18	0.13	0.5	1	1	1
25 Indeno[123-cd]pyrene JPB	ID	0.086	ID	0.0003	0.1	0.009	2.05E-06	4.17E-06	3.51E-10	4.94	5.97	0.13	0.5	1	1	1
26 Benzo[ghi]perylene JPB	ID	0.909	ID	0.0032	0.06	0.01	2.86E-06	4.22E-06	3.56E-10	5.62	6.81	0.13	0.5	1	1	1
27 Beryllium JPB	TDI	2	ID	0.0012	15	NR	NR	NR	NR	NR	NR	0	0.5	1	1	1
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CLEA	Software Version	1.06			Report generated	30-Jan-14				Page 10 of 11
	Environment Agency	Soil-to-water partition coefficient $(cm^3 g^{-1})$	Vapour pressure (Pa)	Water solubility (mg $L^1$ )	Soil-to-plant concentration factor for green vegetables (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soil-to-plant concentration factor for root vegetables (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soil-to-plant concentration factor for tuber vegetables (mg g¹ plant DW or FW basis over mg g¹ DW soil)	Soil-to-plant concentration factor for herbaceous fruit (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soli-to-plant concentration factor for shrub fruit (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soil-to-plant concentration factor for tree fruit (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)
1	Boron JPB	1.00E+01	NR	6.35E+04	0.4 fw	0.2 fw	0.2 fw	0.2 fw	0.2 fw	0.2 fw
2	Arsenic	5.00E+02	NR	1.25E+06	0.00043 fw	0.0004 fw	0.00023 fw	0.00033 fw	0.0002 fw	0.0011 fw
3	Barium	0.00E+00	NR	8.00E+05	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
4	Chromium (III) JPB	4.80E+03	NR	5.85E+05	0.00003 fw	0.00003 fw	0.00003 fw	0.00003 fw	0.00003 fw	0.00003 fw
5	Copper JPB	1.00E+02	NR	1.38E+06	0.0206 fw	0.0206 fw	0.0206 fw	0.0233 fw	0.0206 fw	0.0206 fw
6	Mercury, inorganic	5.00E+02	NR	7.40E+04	0.0038 fw	0.0069 fw	0.0043 fw	0.001 fw	0.0011 fw	0.001 fw
7	Nickel	5.00E+02	NR	2.50E+06	0.0038 fw	0.0043 fw	0.0019 fw	0.0025 fw	0.0025 fw	0.0034 fw
8	Vanadium JPB	1.26E+01	NR	2.11E+05	0.013 fw	0.013 fw	0.013 fw	0.013 fw	0.013 fw	0.013 fw
9	Zinc JPB	3.80E+01	NR	4.32E+06	0.054 fw	0.054 fw	0.054 fw	0.143 fw	0.054 fw	0.054 fw
10	Aromatic >EC16 - EC21 JPB	7.87E+01	5.62E-03	6.53E-01	model	model	model	model	model	model
11	Aromatic >EC21 - EC35 JPB	7.01E+02	1.61E-06	6.61E-03	model	model	model	model	model	model
12	Naphthalene JPB	3.60E+00	2.31E+00	1.90E+01	model	model	model	model	model	model
13	Acenaphthylene JPB	1.01E+01	7.08E-02	7.95E+00	model	model	model	model	model	model
14	Acenaphthene JPB	1.31E+01	7.37E-02	4.11E+00	model	model	model	model	model	model
15	Fluorene JPB	1.57E+01	1.56E-02	1.86E+00	model	model	model	model	model	model
16	Phenanthrene JPB	3.06E+01	2.82E-03	1.12E+00	model	model	model	model	model	model
17	Anthracene JPB	3.13E+01	8.49E-05	5.60E-02	model	model	model	model	model	model
18	Fluoranthene JPB	1.01E+02	1.31E-04	2.30E-01	model	model	model	model	model	model
19	Pyrene JPB	9.03E+01	1.53E-05	1.30E-01	model	model	model	model	model	model
20	Benz[a]anthracene JPB	4.32E+02	1.24E-06	3.80E-03	model	model	model	model	model	model

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	Environment Agency	Soll-to-water partition coefficient $(cm^3g^{-1})$	Vapour pressure (Pa)	Water solubility (mg L <sup>-1</sup> )	Soil-to-plant concentration factor for green vegetables (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soil-to-plant concentration factor for root vegetables (mg g ¹ plant DW or FW basis over mg g ¹ bW soil)	Soil-to-plant concentration factor for tuber vegetables (mg g¹ plant DW or FW basis over mg g¹ bW soil)	Soli-to-plant concentration factor for herbaceous fruit (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soli-to-plant concentration factor for shrub fruit (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soil-to-plant concentration factor for tree fruit (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	
21	Chrysene JPB	3.06E+02	4.52E-08	2.00E-03	model	model	model	model	model	model	
22	Benzo[b]fluoranthene JPB	5.83E+02	6.34E-08	2.00E-03	model	model	model	model	model	model	
23	Benzo[k]fluoranthene JPB	8.24E+02	1.64E-08	8.00E-04	model	model	model	model	model	model	
24	Benzo[a]pyrene JPB	7.17E+02	2.00E-08	3.80E-03	model	model	model	model	model	model	
25	Indeno[123-cd]pyrene JPB	4.85E+02	2.12E-09	2.00E-04	model	model	model	model	model	model	
26	Benzo[ghi]perylene JPB	2.32E+03	1.55E-10	2.64E-04	model	model	model	model	model	model	
27	Beryllium JPB	1.70E+03	NR	1.66E+06	0.007 fw	0.0012 fw	0.0012 fw	0.0012 fw	0.0012 fw	0.0012 fw	
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Environment Agency

Report generated

30-Jan-14

Report title

Edhill Avenue Residential with Plant Uptake - Cd Lifetime

Created by FT at JPB

RESULTS

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	Assessm	ent Criterion	(mg kg <sup>-1</sup> )	Ratio	o of ADE to	HCV		50%	rule?
	oral	inhalation	combined	oral	inhalation	combined	Saturation Limit (mg kg <sup>-1</sup> )	Oral	Inhal
1 Cadmium	1.12E+01	1.85E+02	1.10E+01	0.95	0.05	1.00	NR	Yes	Yes
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Environment Agency	5	Soil Dist	tributio	n							Media	a Concentr	ations					
	Sorbed	Dissolved	Vapour	Total	Soil	Soil gas	Indoor Dust	Outdoor dust at 0.8m	Outdoor dust at 1.6m	Indoor Vapour	Outdoor vapour at 0.8m	Outdoor vapour at 1.6m	Green vegetables	Root vegetables	Tuber vegetables	Herbaceous fruit	Shrub fruit	Tree fruit
	%	%	%	%	mg kg <sup>-1</sup>	mg m <sup>-3</sup>	mg kg <sup>-1</sup>	mg m⁻³	mg m⁻³	mg m <sup>-3</sup>	mg m <sup>-3</sup>	:	mg kg <sup>-1</sup> FW	mg kg <sup>-1</sup> FW	•	mg kg <sup>-1</sup> FW	mg kg <sup>-1</sup> FW	mg kg <sup>-1</sup> FW
1 Cadmium	99.5	0.5	0.0	100.0	1.10E+01	NR	5.48E+00	4.67E-09	5.90E-10	0.00E+00	0.00E+00	0.00E+00	5.70E-01	3.18E-01	3.40E-01	1.76E-01	3.40E-02	1.54E-02
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Environment Agency		Average Daily Exposure (mg kg <sup>-1</sup> bw day <sup>-1</sup> )						Distribution by Pathway (%)							
	Direct soil ingestion	Consumption of homegrown produce and attached soil	Dermal contact with soil and dust	Inhalation of dust	Inhalation of vapour	Background (oral)	Background (inhalation)	Direct soil ingestion	Consumption of homegrown produce and attached soil	Dermal contact with soil and dust	Inhalation of dust	Inhalation of vapour (indoor)	Inhalation of vapour (outdoor)	Background (oral)	Background (inhalation)
1 Cadmium	1.62E-05	1.60E-04	1.19E-07	6.05E-08	0.00E+00	2.51E-04	3.81E-07	4.61	45.34	0.03	0.02	0.00	0.00	49.98	0.02
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Environment Agency		Oral Heatth Criteria Value (µg kg¹ BW day¹)		imaaauon neaan Criteria Value (µg kg¹ BW day¹)	Oral Mean Daily Intake (µg day <sup>-1</sup> )	Inhalation Mean Daily Intake (µg day¹)	Air-water partition coefficient $(K_{aw})$ $(cm^3 cm^3)$	Coefficient of Diffusion in Air $(m^2s^1)$	Coefficient of Diffusion in Water $({\rm m}^2{\rm s}^1)$	$\log K_{\infty} (\mathrm{cm}^3  \mathrm{g}^{-1})$	log K <sub>ow</sub> (dimensionless)	Dermal Absorption Fraction (dimensionless)	Soil-to-dust transport factor (gg <sup>-1</sup> DW)	Sub-surface soil to indoor air correction factor (dimensionless)	Relative bioavailability via soil ingestion (unitless)	Relative bioavailability via dust inhalation (unitless)
1 Cadmium	TDI	0.36	TDI	0.0014	13.4	0.02	NR	NR	NR	NR	NR	0.001	0.5	1	1	1
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Environment Agency	Soli-to-water partition coefficient $(\sigma m^3g^{-1})$	Vapour pressure (Pa)	Water solubility (mg L <sup>-1</sup> )	Soli-to-plant concentration factor for green vegetables (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soli-to-plant concentration factor for root vegetables (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soli-to-plant concentration factor for tuber vegetables (mg g <sup>1</sup> plant DW or FW basis over mg g <sup>1</sup> DW soll)	Soli-to-plant concentration factor store herbaceous fruit (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> bW soil)	Soil-to-plant concentration factor for shrub fruit (mg g <sup>-1</sup> plant DW or FW basis over mg g <sup>-1</sup> DW soil)	Soil-to-plant concentration factor for tree fruit (mg g¹ plant DW or FW basis over mg g¹ DW soil)
1 Cadmium	1.00E+02	NR	1.62E+06	0.052 fw	0.029 fw	0.031 fw	0.016 fw	0.0031 fw	0.0014 fw
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### NB503 Edhill Avenue

Scenarios:

Child Resident - Typical Adult Resident - Typical

Routes:

INGESTION OF SOIL
DERMAL CONTACT WITH SOIL
INGESTION OF ROOT VEGETABLES
INGESTION OF ABOVE GROUND VEGETABLES

Chemicals:

Lead

SUMMARY OF INPUT PARAMETERS	SCENA	RIO: 2
LIFETIME AND BODY WEIGHT Body Weight (kg) Lifetime (years)	15. 6.0	70. 43.
<pre>INGESTION OF SOIL    Soil Ingestion Rate (mg/day)    Exp. Frequency Soil (events/year)    Exp. Duration Soil (years)    Absorption Adjustment Factor for         Ingestion of Soil (-)         Lead</pre>	1.00E+02 3.65E+02 6.0	60. 3.65E+02 43.
Soil Bioavailability (-) Lead	1.0	1.0
DERMAL CONTACT WITH SOIL  Total Skin Surface Area (cm^2) Fraction Skin Exposed to Soil (-) Adherence Factor for Soil (mg/cm^2) Exposure Freq. Soil (events/year) Exposure Duration Soil (years) Absorption Adjustment Factor for Dermal Exposure to Soil (-) Lead	6.70E+03 0.28 1.0 3.65E+02 6.0	1.76E+04 5.00E-02 0.30 3.65E+02 43.
Soil Bioavailability (-) Lead	1.0	1.0
<pre>Exp. Duration Veg. Intake (years) Fraction grown in home garden (-) Koc [(mg/1)/mg/1)]</pre>	51. 14. 1.20E-02 3.65E+02 6.0 0.39	12. 1.20E-02 3.65E+02 43. 0.39
Lead log Kow	ND	ND
Lead Vegetable Uptake Factor [-] (from chemical d Lead	ND atabase) ND	ND ND
<pre>Kd [(mg/L)/(mg/kg)] (from chemical database)</pre>	9.9	9.9



#### MEDIA CONCENTRATIONS

Concentration in Surficial Soil (mg/kg)

Used in calculating carcinogenic risk and hazard index 1.50E+02 1.50E+02 Lead

Conc. in Garden Soil (mg/kg)

This will be the same as surficial soil conc.

Used in calculating carcinogenic risk and hazard index

1.50E+02 1.50E+02 Lead

SLOPE FACTORS AND REFERENCE DOSES

Ingestion Slope Factor [1/(mg/kg-day)]

ND ND Lead

Ingestion Reference Dose (mg/kg-day)

3.60E-03 3.60E-03 Lead

Dermal Slope Factor [1/(mg/kg-day)]

ND ND Lead

Dermal Reference Dose (mg/kg-day)

3.60E-03 3.60E-03 Lead

SCENARIO: SUMMARY OF RESULTS

INGESTION OF SOIL

Daily Doses and Risk for : Lead

CADD (mg/kg-day) 1.00E-03 1.29E-04
LADD (mg/kg-day) 1.00E-03 1.29E-04
Cancer Risk (-) 0.00E+00 0.00E+00
Hazard Index (-) 2.78E-01 3.57E-02

DERMAL CONTACT WITH SOIL

Daily Doses and Risk for : Lead

CADD (mg/kg-day) 1.88E-04 5.66E-06
LADD (mg/kg-day) 1.88E-04 5.66E-06
Cancer Risk (-) 0.00E+00 0.00E+00
Hazard Index (-) 5.21E-02 1.57E-03

INGESTION OF ROOT VEGETABLES

Soil-to-root Concentration Factor, Bvr (mg/mg)

0.0 0.0 Lead

Daily Doses and Risk for : Lead

CADD (mg/kg-day) 0.00E+00 0.00E+00
LADD (mg/kg-day) 0.00E+00 0.00E+00
Cancer Risk (-) 0.00E+00 0.00E+00
Hazard Index (-) 0.00E+00 0.00E+00

INGESTION OF ABOVE GROUND VEGETABLES

Soil-to-above-ground Concentration Factor, Bva (mg/mg) 0.0

Daily Doses and Risk for : Lead

CADD (mg/kg-day) 0.00E+00 0.00E+00
LADD (mg/kg-day) 0.00E+00 0.00E+00
Cancer Risk (-) 0.00E+00 0.00E+00
Hazard Index (-) 0.00E+00 0.00E+00





Site Name	Edhill Avenue
Location	South Shields
Site ID	F1
Job Number	NB503
Date	1/30/2014 12:53:33 PM
User Name	Lafferty@jpb.co.uk
Company Name	Johnson Poole & Bloomer

Hole ID	Sample Depth	Hazardous Waste Y/N	H1	H2	H3A	H3B	H4	H5	H6	H7	H8	H9	H10	H11	H12	H13	H14	H15
_202	0.2m	N	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No
_201	0.7m	N	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No
_205	0.1m	N	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No
_204	0.4m	N	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No
_203	1.1m	N	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No
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Site Name	Edhill Avenue
Location	South Shields
Site ID	F1
Job Number	NB503
Date	1/30/2014 12:53:33 PM
User Name	Lafferty@jpb.co.uk
Company Name	Johnson Poole & Bloomer

Hole ID	Sample Depth	Contaminant	Contaminant Concentration (%)	Hazardous Waste Y/N	Hazard Class	Risk Phrases Exceeded	Additive Risk Phrases Exceeded	H14 Risk Phrases Exceeded	Additional Risk Phrases (see notes section)
_201	0.7m	Benzene	0.0001	N					R11 test
_201	0.7m	Toluene	0.0001	N					R67 (this risk phrase alone will not constitute a waste as being hazardous), R11 test
_201	0.7m	Ethylbenzene	0.0001	N					R11 test
_201	0.7m	m,p-xylene	0.0001	N					R10 test flash point
_201	0.7m	o-xylene	0.0001	N					R10 test flash point
_201	0.7m	Boron	0.002314815	N					R14 (this risk phrase alone will not constitute a waste as being hazardous)
_201	0.7m	Vanadium	0.006605963	N					R55 see comment
_201	0.7m	Free Cyanide	5E-05	N					R12 test
_205	0.1m	Benzene	0.0001	N					R11 test
_205	0.1m	Toluene	0.0001	N					R67 (this risk phrase alone will not constitute a waste as being hazardous), R11 test
_205	0.1m	Ethylbenzene	0.0001	N					R11 test
_205	0.1m	m,p-xylene	0.0001	N					R10 test flash point
205	0.1m	o-xylene	0.0001	N					R10 test flash point
_205	0.1m	Boron	0.001851852	N					R14 (this risk phrase alone will not constitute a waste as being hazardous)
_205	0.1m	Vanadium	0.005356187	N					R55 see comment
_205	0.1m	Free Cyanide	5E-05	N					R12 test
_204	0.4m	Benzene	0.0001	N					R11 test
_204	0.4m	Toluene	0.0001	N					R67 (this risk phrase alone will not constitute a waste as being hazardous), R11 test
_204	0.4m	Ethylbenzene	0.0001	N					R11 test
_204	0.4m	m,p-xylene	0.0001	N					R10 test flash point
_204	0.4m	o-xylene	0.0001	N					R10 test flash point
_204	0.4m	Boron	0.0009259259	N					R14 (this risk phrase alone will not constitute a waste as being hazardous)
_204	0.4m	Vanadium	0.01303339	N					R55 see comment
_204	0.4m	Free Cyanide	5E-05	N					R12 test
_203	1.1m	Benzene	0.0001	N					R11 test
203	1.1m	Toluene	0.0001	N					R67 (this risk phrase alone will not constitute a waste as being hazardous), R11 test
203	1.1m	Ethylbenzene	0.0001	N					R11 test
203	1.1m	m,p-xylene	0.0001	N					R10 test flash point
203	1.1m	o-xylene	0.0001	N					R10 test flash point
_203	1.1m	Boron	0.0009259259	N					R14 (this risk phrase alone will not constitute a waste as being hazardous)
_203	1.1m	Vanadium	0.007677201	N					R55 see comment
203	1.1m	Free Cyanide	5E-05	N					R12 test





#### Notes - Additional Information on Risk Phrases

R1 to R6	Explosive - See comment	Associated with H15, where the hazard (H15) will apply if the waste contains substances that degrade to form, or react with, other wastes or substances (or produce on combustion) other substances with any of the properties H1 to H14, at or above the appropriate threshold.
R7, R8 and R9	Test/calculation for oxides	Applicable to solid compounds that are not explosive, highly flammable, organic peroxides or combustible. A test for the compounds oxidising properties as described in Directive 92/69/EEC, Test Method A17. For organic peroxides calculate the available oxygen content (%). For liquids and oxidising materials not covered by those previously listed no testing available.
R10	R10 test flash point	Flashpoint test as per Directive 92/62/EEC, Test Method A9
R11	R11 test flash point	For liquid substances, undertake the flashpoint test as per Directive 92/62/EEC, Test Method A9. For solid substances undertake flammability test as per directive 92/62/EEC, Test Method A10
R12	R12 test flammability	Flammability of gasses test as per Directive 92/62/EEC Test Method A11.
R15	R15 test flammability	To test the flammability of a substance when in contact with water test as per Directive 92/62/EEC, Test Method A12.
R16	R16 test for explosives	See comment above
R17	R17 pyrophoric test	To test the pyrophoric properties of solids and liquids test as per Directive 92/62/EEC, Test Method A13.
R18	R18 test for flammable explosive vapour air mixture	See comment above
R19	R19 test for flammable explosive peroxides	See comment above
R29	R29 test or calculation	Undertake test as per Directive 92/62/EEC, Test Method A12.
R31	R31 test or calculation	Undertake testing as per Directive 92/62/EEC, Test Method A12 modified to replace water with an acid which will not cause a displacement reaction to occur. Method to measure SO2 evolved when a waste is in contact with an acid (see Environment Agency SWEN 068).
R32	R32 test or calculation	Undertake testing as per Directive 92/62/EEC, Test Method A12 modified to replace water with an acid which will not cause a displacement reaction to occur).
R44	R44 test for explosives	See comment above
R54 to R58	see comment	Classification of waste as ecotoxic (on the basis of terrestrial non-aquatic toxicity) is not applicable due to the lack of detailed information. Until more data becomes available R54 to R58 should not be considered when assessing the ecotoxic hazard of wastes and classifications should be based upon aquatic toxicity data. Where there is reason to believe that a waste contains substances that only have effects on the terrestrial environment, guidance on the approapriate test method should be obtained from the Environment Agency.

#### Notes

Testing of compounds which would be classified under H14 should only be undertaken where the hazards cannot be adequately identified. (i.e. where the waste contains a substance/s for which there is no aquatic toxicity data and/or where the waste is an uncharacterised mixture and/or there is the potential that the waste may contain unknown substances or breakdown products.

Aquatic toxicity testing should be undertaken in accordance with the Environmental Health and Safety Publication, series on Testing and Assessment No. 23 ENV/JM/MONO(2000) 6 June 2000



#### JPB Methodology for Exposure Assessment

#### **Regulatory Framework**

The assessment of potentially contaminated sites and the associated risk to the proposed development is dependent on a number of factors namely, the intended site end use, distribution and level of contamination, characteristics of the soil (i.e. pH, permeability) the groundwater regime and the sensitivity of the surrounding area. An analysis of the interaction between these various factors allows a decision to be made with regard to the extent of any remedial measures required for the development.

The contaminated land provision of the Environment Protection Act 1990, inserted by Section 57 of the Environment Act 1995, came into force in July 2000. This guidance has been revised and came into force on 6 April 2012. Within this "Contaminated Land" is defined as

"any land ....... in such a condition by reason of substances in, on or under the land, that

- a) significant harm is being caused or there is a significant possibility of such harm being caused; or
- b) pollution of the water environment is being, or is likely to be caused;"

In addition "the questions

- a) what harm or pollutant of the water environment is likely to be regarded as significant
- b) whether the possibility of the significant harm or significant pollution of all the water environment being considered significant"

In addition, the National Planning Policy Framework, issued March 2012, sets out the Government's planning policies for England. This framework also requires a "suitable for use approach" which requires remediation only where there are unacceptable risks to health and the environment depends on the current and proposed end use.

In addition, the guidance requires a significant pollutant linkage to be present which includes;

- A source (pollutant)
- A pathway
- · A receptor

JPB has therefore developed a risk assessment approach based on this philosophy, the methodology used is represented diagrammatically in the attached flow chart.

#### Stage 1 - Preliminary Risk Assessment-

#### Desk Study

The methodology utilised for desk studies follows the specifications outlined in CLR2 "Guidance on Preliminary Site Inspection of Contaminated Land", CLR6 "Prioritisation and Categorisation Procedure for Sites which May be Contaminated" and BS 10175: 2001 "Investigation of Potentially Contaminated Sites – Code of Practice", BSI 2001.

During the study, documentary research will include an examination of the Ordnance Survey maps for details regarding previous site and adjacent land uses. Similarly the available geological maps will be examined to determine the geological/hydrogeological conditions beneath and adjacent to the site. In addition, regional memoirs will be consulted together with mine abandonment plan data and any available borehole records, in order to assess the mining conditions. A walkover survey will be carried out to determine the existing site conditions and operations. In addition, a photographic record of the site is taken during the walkover survey. Information will also be obtained from the EA website and a review of in-house information. A Report of environmental database information may also be obtained.

#### Conceptual Site Model

A Conceptual Site Model (CSM), which describes how potential chemical sources at the site could contribute to increased levels of risk to potentially sensitive receptors, is developed at an early stage and constantly reassessed in light of investigative findings. CSMs are generated in accordance with Guide to Good Practice for the Development of Conceptual Models and the Selection and Application of Mathematical Models of Contaminant Transport Processes in the Subsurface - National Groundwater & Contaminated Land Centre report NC/99/38/2 – Environment Agency 2001. The first step in developing such a model is to identify whether there are potential hazards which may pose a risk on the site through desk top research and professional judgement. In addition, information regarding the site-specific environmental setting including geology, hydrogeology, hydrology etc, is gathered in order to assess the potential exposure pathways which are likely to exist and the location of humans and environmental resources which could be impacted by the site.

Following this desk based study and the development of a CSM a site investigation is designed in order to determine whether any potentially significant pollutant linkages actually exist on the site. The information gathered during the investigation is then used to revise the CSM and as the basis of the risk assessment process. While any investigation strategy will be specific to each site the following general comments can be made.

#### Design of Site Investigations

JPB designs and implements site investigations in accordance with BS10175. Care is taken to target investigations at potentially contaminated locations identified in the CSM from researches and from site visits or other available information. In addition, during the performance of investigations locations are refocused in the light of known site conditions. Further investigations are also undertaken at randomly selected locations resulting in a mixture of random and targeted investigation locations.

The requirement for adequate site coverage is a key consideration at the design stage and the number and type of investigation locations is determined by the available information, the brief and the requirements of the guidance given in CLR4 and R & D Publication Report P5-066/TR Secondary Model Procedure for the development of Appropriate Soil Sampling Strategies for Land Contamination. BS10175 indicates that in order to provide adequate site coverage a sampling grid of between 20m and 25m should normally be applied where residential development is considered. Where the CSM indicates there to be no potential source of contamination on the site, or other land uses are envisaged, a 50m spacing may be adopted.

Investigations are designed such that, in statistical terms, the number of sampling points investigated would identify a "hot spot" zone of contamination covering 5% or greater of the site area. On small sites where this is impractical, the design of investigations is such as to determine that a hotspot of a certain area does not go undetected.

Site-Specific Risk Assessment

#### Site Zoning

Some sites may need to be divided into geographical sectors where, for example, historical land uses differ or the type of development varies across the site in accordance with R & D Technical Report P5-066/TR. Good practice guidance describes averaging areas as "areas of soil to which a receptor is exposed or which otherwise contributes to the creation of hazardous conditions". Where made ground material is contaminated at variable concentrations, but within a single geological unit JPB considers that this unit can be adopted as an averaging area for the purposes of making an assessment of human health risks. However, where measured contamination concentrations include statistical outliers of high concentration, where different historical land uses have resulted in different patterns of contamination or where there is a clear distribution of higher contaminant concentrations in one sector of the site, averaging areas are chosen to reflect this contaminant distribution. Single high contaminant concentrations may indicate the presence of "hotspots" which may merit closer scrutiny or additional investigation.

Investigation locations such as trial pits and boreholes are positioned to provide adequate site coverage, where access is available and avoiding existing services. Boreholes are situated at a mixture of targeted and random locations at the site where access is possible. During the investigation the sampling strategy in CLR 4 "Sampling strategies for contaminated land" together with the guidance given in R & D Publication Report P5-066/TR is followed. The rationale behind the sampling strategy given in the R & D publication is:

Depth of sample	Rationale
0-0.5	To assess
	<ul> <li>Human/animal intake arising from ingestion and dermal contact</li> <li>Potential for wind entrainment leading to inhalation (of contaminated soils and dusts) or deposition onto neighbouring land</li> <li>Surface water run-off (e.g. due to flash flooding)</li> <li>Uptake by shallow rooting plants (e.g. crops, ornamental and wild species)</li> <li>Surface leaching to groundwater.</li> </ul>
0.5m in made or natural	To assess
ground	<ul> <li>Intake via ingestion/inhalation/dermal contact from "abnormal" )or unpredicted) excavation (e.g. children digging dens) or for other purposes such as swimming pools, ponds house extensions)</li> <li>Uptake by deep rooting shrubs and trees</li> <li>Intake by, or arising from, the activities of burrowing animals</li> <li>Intake arsing from construction / maintenance of buildings and services for example.</li> <li>Foundations (usually within 2m of formation level</li> <li>Water supply pipes, telecommunications, gas &amp; power (0.5-1m of final formation level)</li> <li>Sewers (from 0.5 &gt; 1m of final formation level)</li> </ul>
	To locate perched water or groundwater To confirm depth of made ground To locate possible lateral pathways for gas or vapour migration in made ground To establish extent of any leaching of soluble constituents from superficial soils To detect "deep" contaminants (e.g. gas generating materials, leachable materials, dense solvents located on top of an impermeable stratum) To obtain information of "background" soil properties To locate "natural" lateral migration pathways.

Samples are generally taken at shallow depth, then at relevant changes in material with depth. Where any made ground is thick and relatively uniform samples are taken every 0.5m to 1.0m. A sample of natural soils is generally taken from beneath each made ground horizon where the base is proven. Samples are recovered from each trial pit Samples are recovered at these regular intervals with additional samples of any atypical horizons also taken. It should be noted that there will always be the possibility of additional unrecorded conditions outwith the sampling points. Samples obtained are stored within appropriate containers and dispatched for analysis within 24 hours of sampling.

Attempts are made to recover water samples from all of the boreholes at which standpipes are installed. Each borehole is extensively purged to a volume in excess of three times the well volume using a submersible mini-whale pump. Purging before sampling allows a more representative water sample of groundwater to be obtained and ensures that any water initially present in the boreholes is removed as this may have been chemically altered due to reaction with air or with installation materials. Water samples are transferred to appropriate containers before being transported to the testing laboratory in cooled conditions.

Testing parameters scheduled on soil and water samples are based on historical and current operations information and their importance in relation to health risks, phytotoxicity, impact on the water environment, protection of building materials, services and structures from chemical attack and potential impact on the quality of potable water supplies. Where possible chemical testing is targeted at locations at the site where particular contaminants are anticipated. Selection of test parameters is performed on a site specific basis as described in the text of each investigation report.

#### Stage 2 Generic Quantitative Risk Assessment

The next stage of the site-specific assessment is to perform a Stage 2 risk assessment using the information gathered during the site investigation to determine the actual nature and extent of contamination, evaluating the data using conservative generic criteria to determine whether any recorded levels of contaminants could be potentially of concern.

#### Stage 2 Criteria

The Stage 2 generic quantitative assessment of risk to human health, property, ecology, surface water and ground water considers the potential for exposure based on comparison of the results to conservative generic criteria.

In terms of human health the results of the soil testing are assessed with reference to the guidance published by DEFRA and the Environment Agency including; Soil Guideline Values (SGVs) derived using the CLEA model and the methodology described in EA Science Report SC050021/SR3, EA CLEA science reports and the associated TOX and SGV series of reports. Based on this guidance JPB has calculated a series of generic assessment criteria (GAC) for different land use scenarios. Where no data are available from these sources, an automatic Stage 3 assessment is carried out if the parameter is present above laboratory reporting limits. The guideline concentrations appropriate to the proposed end use of the site is used in the interpretation of the results. At Stage 2 all soil contaminant concentrations are compared with GACs. If necessary, at Stage 3 representative soil contaminant concentrations are calculated and used for comparison with assessment criteria.

To assess the site's potential for phytotoxicity JPB refers to the MAFF/DoE document "Review of the Rules for Sewage Sludge Application to Agricultural Land – Soil Fertility Aspects of Potentially Toxic Elements" in the absence of other definitive phytotoxic screening levels. This document is authoritative and scientifically based, it sets out total concentrations of various metallic elements which shouldn't be exceeded in order to maintain soil fertility and avoid toxicity. Therefore it is considered that these limits can be applied to contaminated land and other situations, e.g. they have been adopted by DEFRA in its "Soil Code" and by the Forestry Commission. It should be noted that plant growth can also be significantly affected by many other factors including: pH, nutrient availability, soil texture and structure, temperature, moisture content and aeration. In addition reference has been made to "Soil Code" (MAFF 1998), and CLR2, "Guidance on Preliminary Site Inspection of Contaminated Land".

#### Structures and Services

Where structures or services are considered to be viable targets, risks are assessed using contemporary best practice guidance given in documents published by the Building Research Establishment (BRE), CIRIA, Water Research Council (WRc), WRAS the HSE and other relevant organisations.

Risks posed to buildings and services due to aggressive soil sulphate, chloride and pH conditions are assessed using the guidance given in BRE Special Digest 1 (2005), Concrete in aggressive ground.

#### Water Supply Pipes

Risks posed by soil and groundwater contaminant concentrations to water supply pipes are assessed in accordance with the UK Water Industry Research (UKWIR) document, "Guidance for the Selection of Water Supply Pipes to be used in Brownfield Sites", UKWIR report reference 10/WM/03/21, 2010. This guidance identifies the chemicals present in soils which can either permeate pipes or impact on their integrity by causing swelling, cracking and degradation or corrosion. The main focus is, therefore, on organic contaminants and on the soil's conductivity, pH and redox potential.

Where a site has been greenfield and no chemicals have been historically or currently stored or used on it (or part of the site meets these criteria), no restriction is made on the type of water pipes which can be used on the site (or part of the site as appropriate). In these circumstances the water company may require that a PID survey of the route of water supply pipes is undertaken, extending to 15m either side of the pipe route, in order to confirm that no unexpected chemical contamination is present. Alternatively this requirement can be satisfied by upgrading pipe materials to PE-Al-PE barrier pipe, which would be protective of water supplies.

It should also be noted that where the site is within close range of a petrol station or other fuel storage facility, the water company may require that the water supply pipes installed take account of future contamination risks from these adjacent sources.

Where the site is brownfield or where chemicals have been stored or used, samples are obtained from locations on site as identified in the site CSM. Where the route of water supply pipes is known, sample locations during investigations would include locations on or within 15m either side of the route, otherwise investigation coverage for the whole site is as described previously in this methodology and as recommended in section 2.5.5 of the UKWIR report.

Selected soil samples are tested for the parameters recommended in the UKWIR guidance; VOCs (including TIC), SVOCs (including TIC), petroleum hydrocarbons (including "mineral oils"), conductivity, pH value and redox potential. Results of analyses are collated and compound group concentrations summed as described in section 2.7.9 of the UKWIR guidance, these sums are adopted as Representative Contaminant Concentrations (RCCs). The maximum concentration recorded at the site (or if appropriate within a particular site zone) for each substance is used for summing and tabulation, this is a conservative assumption.

The RCCs are compared with the UKWIR threshold values for polyethylene (PE) and polyvinylchloride (PVC pipes) detailed in Table 3.1 of the UKWIR, which have been adopted as JPB GACs. Exceedance of a single GAC indicates PE or PVC pipework is not appropriate and other pipe materials should be selected. Consideration of the corrosive properties of soils is also required where PE, PVC or barrier pipes are not selected as appropriate. The comparison of RCCs with GACs and the other criteria in Table 3.1 of the UKWIR guidance results in a list of pipe materials which would be suitable in terms of chemical properties, a preferred selection can then be made on the basis of cost, appropriateness etc. or the choice of specific materials to be used made by the engineer/developer. Further recommendations on standards and specifications for water supply pipes and fittings for various pipe materials are given in Part 4 of the UKWIR guidance.

#### Combustibility

Where potentially combustible materials are encountered the following assessment methodology is adopted. Despite the potential for combustion in many sites characterised by carbonaceous materials, the number of recorded instances of actual combustion are very few and there has been no definitive study of the phenomena. Consequently, there are no commonly accepted criteria for comprehensively assessing and dealing with the risk of spontaneous combustion. The ICRCL Guidance Note 61/84 "notes on fire hazards of contaminated land" suggests that there is an unacceptable risk of combustion if the material has a Calorific Value in excess of 10 MJ/kg or perhaps only 7 MJ/kg.

However a paper presented at the Fourth Mineral Waste Utilisation Symposium related to the Utilisation of Coal Refuse for Highway Base or Sub-base Material. In this paper it states that "low permeability values are desirable in order to reduce air circulation and the potential for spontaneous combustion". It then goes on to suggest that "proper compaction of coal refuse reduces air voids to less than 10% and the potential for spontaneous combustion is substantially reduced".

There is an imprecise relationship between Loss on Ignition and Calorific Value but previous comparisons by JPB has indicated 10 MJ/kg to be roughly equivalent to 30% Loss on Ignition and 7 MJ/kg to be roughly equivalent to 23% Loss on Ignition.

JPB adopts the following guidelines:

- i) combustion may be induced and supported only if the Loss on Ignition value exceeds about 20% and the Calorific Value exceeds 7 MJ/kg.
- ii) carbonaceous material needs to be of some bulk ie thicker than 1 metre and greater than 10 m<sup>3</sup> in volume.
- iii) spontaneous combustion should not occur in thoroughly compacted material to which air is excluded.

#### Water Environment

Current SEPA guidance described in document WAT-PS-10-01: Assigning Groundwater Assessment Criteria for Pollutant Inputs (March 2010) notes that for land contamination four receptors were to be assessed, if identified as being present, namely surface water; groundwater abstraction; groundwater resource; and groundwater dependant terrestrial ecosystem (GWDTE or wetland). Routine leachability testing is carried out for water soluble contaminants in order to determine if there is a threat from soil borne contaminants to ground and surface waters.

For the protection of surface waters and groundwater resources the concentration of each contaminant in soil leachates, groundwaters and surface waters are compared against relevant assessment limits. The assessment limits may be a UK Drinking Water Standard (UKDWS), Resource Protection Value (RPV) or EQS depending on the nature of the receptor which is being considered to potentially be at risk.

Where no assessment limit has been provided other limits may be adopted such as WHO Drinking Water Guidelines, US EPA National Primary Drinking Water Regulations or the laboratory's minimum reporting limit (MRL).

#### Stage 2 Risk Evaluation

Stage 2 risk based guidance levels are conservative generic values against which measured contaminant concentrations can be compared. Where measured concentrations are found to be below these screening criteria then the contamination identified is not considered to pose a significant risk. The guidance used to evaluate investigation data is chosen to be relevant for the particular risk and receptor being assessed as well as being applicable to the legislative issues of concern. Where measured concentrations of contaminants exceed generic criteria the risks posed by the contaminants of concern are considered more fully in a Stage 3 risk assessment. Where no generic criteria are available or a substance, an automatic Stage 3 assessment is carried out if the contaminant is present above laboratory reporting limits.

Stage 2 criteria adopted by JPB for risk assessments are appended. If any of the appropriate criteria contained in these documents are exceeded, the conclusion is that significant risk could exist and that a further assessment (Stage 3) is warranted in order to calculate the potential levels of risk. This process therefore focuses on the contaminants of concern and can, if necessary, inform any further investigations which may be required for more detailed examination.

#### Stage 3 Detailed Quantitative Risk Assessment

#### Assessment of risks to human health

Each contaminant exceeding Stage 2 criteria is examined for its potential to cause harm. Consideration is then given to the significant pollutant linkages which are plausible for the identified hazards, i.e. whether a contaminant can conceivably come into contact with a specified target group. It is possible that a contaminant may be deemed a hazard due to its presence above screening criteria but ultimately not constitute a risk as no viable pathway exists between the source and the receptor. The relative sensitivity of all potential receptors identified is quantitatively assessed using the data obtained during the desk study and site investigation phases.

The risk to human health is determined using an exposure assessment, an estimate of potential doses of the chemicals in exposed individuals via the pathways identified in the Conceptual Site Model. This focuses on a hypothetical individual within each exposed population and involves the use of models which incorporate assumptions regarding human behaviour and physiological attributes. The assumptions are made in a "worst case" or "reasonable worst case" manner to provide estimates of dose which are unlikely to be exceeded by receptors at or in the vicinity of the site. The main focus of the exposure assessment is the estimation of long-term (chronic) dose levels from repeated exposure to chemicals in the soil and groundwater. Exposure to each chemical is estimated for each viable pathway and for any potential sensitive receptors.

The purpose of the human health assessment is to identify the levels of exposure to contaminants which, if not exceeded, do not cause adverse health effects. The subject of human health assessments is covered in depth in the DEFRA/EA Science reports to which the reader is referred for further background information, but a short review is given below.

#### Health Criteria Values

Human health assessment criteria are derived by comparing the estimated exposure of critical receptors to the contaminants with Health Criteria Values (HCVs) that represent a tolerable or minimal risk to health from chronic exposure to these contaminants (acute health risks must be assessed separately). Health Criteria Values are derived through the collation and review of toxicological data and its subsequent use in the derivation of soil contaminant intakes that are considered to be protective of human health. These intakes are guidelines to a risk assessor on the level of long-term human exposure to individual chemicals in soil that are tolerable or pose a minimal risk. HCVs are established from a review of the evidence from occupational and environmental epidemiological studies, animal studies, and from scientific understanding of the mechanisms of absorption, transport, metabolism and toxicity of chemicals within the human body. The derivation of HCVs is described in detail within EA Science report-SC050021/SR2.

Contaminants generally exhibit two possible types of toxicity, threshold toxicity and non-threshold toxicity. For contaminants which exhibit threshold toxicity there is some, non-zero, measurable amount of exposure (dose) that is required before a biological threshold is breached and an adverse health effect is produced. However, in some cases the toxicological mechanism responsible for producing the adverse effect is such that there is no basis to assume a threshold exists. This is most notably the case for genotoxic carcinogens. The biological mechanisms by which these types of chemicals cause damage to DNA and genetic material means, that any exposure to these chemicals, no matter how small, will carry some level of risk. The theoretical basis for this is that one 'hit' on DNA can produce a mutation that may eventually lead to a tumour. It is therefore not possible to identify the threshold with any confidence. Hence, the prudent assumption is made that such compounds do not have a threshold. It should be noted that not all carcinogens are genotoxic, some may exhibit a threshold, and whether a contaminant is a threshold or non-threshold substance should be determined by a review of the available toxicological evidence.

HCVs for threshold substances are referred to in the UK as Tolerable Daily Intakes (TDIs), some other authorities or organisations derive similar criteria such as Reference Doses (RfDs) or Provisional Tolerable Weekly Intakes (PTWIs). These values are in principle similar and can be thought of as "safe" levels of exposure at which adverse effects are not likely to occur, although some conversion or further consideration may be required before adoption in the UK context. These health criteria are typically derived by applying "safety" or "uncertainty" factors to intake levels observed to have little or no effects in humans or animals.

Exposure to receptors will occur not just from soil-borne contamination but also due to intakes from food, water and air. Where a contaminant is a threshold substance these background intakes of a contaminant must therefore be calculated and subtracted from the TDI, to calculate the intake of the contaminant which could be tolerated from exposure to soil contamination alone (this quantity is the TDSI – Tolerable Daily Soil Intake), in addition to normal background exposure. This background intake is the Mean Daily Intake (MDI). Where information is not available on intake levels of contaminants or where the MDI exceeds the TDI, the Science report-SC050021/SR3 states that the TDSI should be set in the model to be 50% of the TDI.

DEFRA/EA has adopted the Index Dose (ID) as the HCV for non-threshold substances, which can be considered to present a minimal human health risk from exposure to soil contaminants. For non-threshold contaminants background intake is not considered as there is no "safe level". In addition, application of the ALARP (As Low As Reasonably Practicable) principle for these substances means that intake should be reduced to as low a level as practicable, that this principle is being adopted by the competent authorities for intakes from food, water and air and that actions are being taken to reduce these other intakes.

There are a number of sources of toxicity criteria and background exposure levels which include Department of the Environment, Food and Rural Affairs (DEFRA); World Health Organisation (WHO); the US Environmental Protection Agency (US EPA) IRIS (Integrated Risk Information System) and other published scientific literature. Where available the definitive UK toxicological and background exposure levels published in the DEFRA/EA/SEPA CLEA TOX reports, under the advice of the Department of Health and The Food Standards Agency, are used as the primary source. However, as authoritative UK based information is available for only a limited number of substances, health criteria and other model input data has been sourced from non-UK published information. The methodology outlined in Science report-SC050021/SR2 has been used to derive HCVs where an authoritative UK HCV has not been published.

#### General Approach to Risk Estimation

At Stage 3 where concentrations of contaminants have exceeded Stage 2 generic criteria or in the absence of generic criteria, JPB has used the CLEA 1.06 model to derive SSACs (Site-Specific Assessment Criteria), where sufficiently reliable UK authoritative or peer-reviewed input data (including HCVs) is available. The model input values published by DEFRA/EA, derived by Land Quality Management (LQM) in association with the Chartered Institute of Environmental Health (CIEH) and data published in Environment Industry Commission (EIC)/CL:AIRE Report: Soil Generic Assessment Criteria for Human Health Risk Assessment have been used for this purpose. The CLEA 1.06 model derives SSACs for use when considering the risk to human health from chronic exposure to toxic metals, metalloids and organic substances in soil. The assessment criteria represent contaminant concentrations in soils, which if exceeded on site may be indicative of unacceptable risks to human health. It is envisaged that this methodology can be used as a tool during either the detailed quantitative risk assessment or the risk management process.

The model adopts the risk-based source-pathway-receptor pollutant linkage framework and a deterministic methodology. The exposure pathways considered are direct ingestion of soil and dust, direct dermal contact with contaminated soil, consumption of home grown or allotment vegetables, ingestion of soil attached to such vegetables, inhalation of soil vapours outdoors and inhalation of soil vapours indoors. The model is intended to reflect and be compliant with the guidance in DEFRA/EA Science Reports.

Where input data from the above sources is not available, data published by other organisations has been used. It should be noted that the toxicological data available for particular substances in many cases is very limited and incomplete. In order to adopt a relatively consistent approach, where authoritative or peer reviewed UK data is not available, data has been obtained primarily from USEPA and Dutch RIVM report sources as these sources offer a wide range of expert reviewed parameter values such as health criteria values, physical and chemical property data for commonly encountered soil contaminants.

### Risks posed by Lead in soil

DEFRA guidance to date has advocated assessing risks posed to human health by lead in soils using an HCV set at a blood lead level of 10µg/dL and deriving an SGV using the Society for Environmental Geochemistry and Health (SEGH) model. EA are currently working on revised TOX and SGV reports for lead and have stated that when they update the HCV and SGV for lead, they will consider setting the HCV as an intake dose. This will allow the use of the CLEA model to calculate the SGV and its use for site-specific risk assessments. These documents have not been published to date, therefore, the previous SGVs published in DEFRA/EA R&D Publication SGV 10 have been adopted in the interim.

#### Risks posed by Polychlorinated biphenyls (PCBs) in soil

For risk assessment purposes PCB congeners are divided into two groups; (1) dioxin-like PCBs and (2) non-dioxin like PCBs. Dioxin-like PCBs have similar structures and toxic mechanisms to dioxins and furans and so are assessed together with dioxin and furans. Non-dioxin like PCBs have a different toxic end point to dioxin-like PCBs and must therefore be assessed separately.

If the criteria set out in the SGV report are fulfilled, the PCB test results can be directly compared with the SGV given in the report. However, SGVs relate to background PCB levels where a site source is absent, and this limits the applicability of the SGV.

Where the assumptions required for the use of the SGV are not met, dioxin-like PCBs are assessed using the SGV worksheets for the standard land uses. Where site specific dioxin and furan data is not available, the median urban or rural dioxin and furan values given in the SGV report are used to account for "background" concentrations of these substances. A hazard index (HI) is calculated using the worksheet and if the HI is >1, then dioxin-like PCBs may pose a risk to human health receptors in the scenario being considered.

A specific methodology to assess risks posed by non-dioxin like PCBs has not yet been published by EA/DEFRA, however, JPB has adopted the current UK methodology used to assess other organic compounds. This involves selecting a list of target compounds, a TDI and other input data and using the CLEA model to derive GACs. PCBs are typically present as mixtures. The most persistent and toxic non-dioxin-like PCBs are present at their highest concentrations in PCB mixture aroclor 1254. The 7 ICES list indicator PCBs make up about 50% of aroclor 1254. JPB therefore compares the sum of these indicator PCBs with the assessment criteria. The criteria are derived using a TDI for aroclor 1254 and other input data using the CLEA model. The TDI is adjusted to account for the percentage of the 7 ICES compounds present in aroclor 1254. If the sum of the soil concentrations of the 7 ICES exceeds the GAC, then non-dioxin-like PCBs may pose a risk to human health receptors in the scenario being considered.

Therefore, if either the dioxin-like PCB or non-dioxin-like PCB assessment indicates the presence of a risk, remediation may be required or a further assessment may be proposed.

#### Risks posed by Cyanides in soil

Cyanide compounds exhibit both acute and chronic toxicity, although it should be recognised that complex cyanides are much less toxic than free cyanides. There is currently no UK SGV available to assess chronic cyanide toxicity, although a review of the toxicology of cyanide has been published (DEFRA CLR TOX 5 report).

Criteria derived to be protective of chronic cyanide exposure exceed those derived to be protective of acute exposure to both types of cyanide. Therefore, the criteria derived for acute exposure to free and complex cyanides have been conservatively adopted to be protective to receptors. The Environment Agency has not published guidance on the assessment of risks due to acute exposure to cyanide compounds. However, HPA publications indicate that hydrogen cyanide and its solutions may be fatal following acute exposure via all intake routes (ingestion, inhalation and dermal). The Committee on Toxicity of Chemicals in Food, Consumer Products and the Environment (COT) published a nominal acute reference dose (ARfD) of 5µg CN per kilogram bodyweight (µg/kg bw-¹) based on the lowest reported acute lethal dose (range of 0.5 – 3.5 mg/kg bw-¹) multiplied by a 100 fold uncertainty factor: 10 to account for inter-individual variability; and, taking into account the steep dose-response relationship for cyanide, 10 to extrapolate from an effect level.

To derive an assessment criteria for free cyanides from the above ARfD, a 2g bolus dose of soil is assumed to represent a reasonable worse case acute ingestion intake for a sensitive receptor: for residential scenarios this is a female child with a body weight of 9.8kg (default value for Age Class 2), for a commercial/industrial scenario it is a female adult worker with a body weight of 70kg (default value for Age Class 17). An SSAC for free cyanides is then calculated for the sensitive receptor based on the mass of cyanide it would be necessary for the receptor to consume via soil ingestion in order to reach the ARfD for their body weight.

Cyanide contamination in soil has been reviewed by the Dutch RIVM organisation who have derived HCVs for chronic exposure to cyanides of 50 and 800µg for free and complex cyanides respectively, a ratio of 1:16 between the two forms of cyanide. The ratio of free cyanides to complex cyanides is based on evidence reviewed by RIVM indicating that interconversion between complex cyanides and free cyanides occurs at a relatively low rate. RIVM also provide evidence that complex cyanides are poorly absorbed from the gut with only limited dissociation of absorbed complex cyanides to toxic HCN or CN. Therefore, although the Dutch HCVs are higher than the UK values, the ratio of free cyanides to complex cyanides is considered to be applicable as it is based on bio-accessibility considerations. Adjusting the UK free cyanides ARfD by a factor of 16, results in a calculated complex cyanides ARfD, of 80µg CN/kg bw. An SSAC for complex cyanides is then calculated for the sensitive receptor based on the mass of cyanide it would be necessary for the receptor to consume via soil ingestion in order to reach the adjusted ARfD for their body weight.

#### Representative Contaminant Concentrations and Site Specific Assessment Criteria

At this stage the chemical dose to potentially exposed human receptors are calculated, incorporating site specific data together with conservative health assumptions where necessary to derive Site Specific Assessment Criteria (SSACs). Data evaluation and statistical procedures are used to derive representative contaminant concentrations (RCC) for contaminants of concern in the relevant averaging areas of sites. RCCs are compared with SSACs at the risk evaluation stage in order to determine their significance. This process effectively reduces the conservatism of the Stage 2 assessment and provides a site specific assessment at Stage 3.

At Stage 2 all soil contaminant concentrations are compared with GACs. At Stage 3 RCCs are calculated and used for comparison with assessment criteria. Depending on the nature of the data the RCC may consist of either the maximum concentration recorded or a 95% Upper Confidence Limit (UCL95). Where small data sets are available, or where point source contamination such as hydrocarbon spillages are present, statistical analysis is not appropriate and the maximum contaminant concentration recorded is adopted as the RCC. Where larger data sets are available statistical analysis may be performed to derive an RCC where appropriate. Where RCCs exceed assessment criteria this indicates that the contaminant poses a human health risk and that remedial actions may be required to prevent actual harm.

Statistical analysis is carried out in accordance with the methodology outlined in guidance given in CL:AIRE/CIEH Publication, "Guidance on Comparing Soil Contamination Data with a Critical Concentration". A number of statistical tools may be used for deriving UCL95 values, JPB principally uses ProUCL, a software package developed by the US EPA for this purpose. In general RCC values are selected as follows;

- Determine if there is sufficient data for statistical analysis, if not the maximum concentration is selected as the RCC.
- If data is sufficient the data set for each contaminant is tested for distribution type (normal distribution, lognormal etc.);
- The data set for each contaminant is tested for the presence of outliers, and these are considered for removal or inclusion in further calculations;
- An appropriate UCL95 is calculated, based on the distribution type and revised data set, and this is used as the RCC.

Consideration of whether outliers represent potential contaminant hotpots is also undertaken.

As previously indicated, lead risks are assessed using an SGV derived using the SEGH model, which uses the geometric mean of blood lead levels as one of its input parameters. For this reason the log transformation of soil lead concentrations across a site is required prior to deriving the RCC.

#### Stage 3 JPB Risk Estimation Practice

JPB's Stage 3 assessment practice is to calculate SSACs, incorporating site specific data together with conservative health assumptions where necessary. This effectively reduces the conservatism of the Stage 2 assessment and provides a site specific assessment. Depending on the pollutant linkages identified in the conceptual site model and on the nature of contamination identified during site investigations, particular risk assessment tools are selected which are considered to be appropriate to assess risks to human health under the existing site conditions. In general JPB most frequently uses the CLEA 1.06 model, or the RISC4 risk assessment tool.

The CLEA 1.06 model has been designed to comply with current UK DEFRA guidance on the assessment of contaminants on land and where possible this is JPB's risk assessment tool of choice. Health criteria, toxicological, physical and chemical data are input for each contaminant for the land use envisaged. The model derives a Site-Specific Assessment Criteria (SSAC) for the contaminant which, if exceeded, would represent a human health risk to the sensitive receptor. The basis of the CLEA 1.06 model is more fully discussed in the CLEA software manual.

The RISC4 model compares risk estimates with acceptability criteria at the risk evaluation stage in order to determine their significance. It is considered that a **Human Hazard Index in excess of 1.0** is significant and an **increased lifetime cancer risk in excess of one in hundred thousand (10**.5) is considered to be significant, subject to the guidance in Science report-SC050021/SR2. Risk estimates for contaminants exceeding these criteria are considered to indicate that the contaminant poses a human health risk and that remedial actions may be required to prevent actual harm. JPB may chose the RISC4 risk assessment tool to carry out assessments as RISC4 allows the modelling of a wide range of exposure pathways, is compliant with the Risk Based Corrective Action (RBCA) philosophy and has been the subject of a comparative bench marking study carried out by the Environment Agency. The basis of the RISC4 model is discussed further in the RISC4 software manual. Where the model allows, the RISC4 input parameters are amended by JPB to reflect the guidance and inputs of the CLEA reports.

The CLEA 1.06 model used to derive SGVs, GACs and SSACs includes inhalation of outdoor and indoor dust pathways where appropriate. Inhalation pathways are most important in driving risk assessments where inhalation HCVs are low or where inhalation exposure is high. Where a Stage 3 assessment is required, the inhalation SSACs are presented in JPB's reports to allow further consideration of these pathways and any remedial actions which may be required.

On completion of contemporary developments the amount of bare soil exposed is generally limited to localised landscaping. This is considered to be minimal as a proportion of the site area and given that clean topsoil will generally be placed to provide a suitable rooting horizon during development, this pathway will be usually be broken by this cover for most inorganic contaminants and therefore JPB does not assess this further. An additional degree of conservatism is build into the assessment here as the overall SSACs still have these pathways included. However, where volatile organic contaminants are present, such as BTEX or naphthalene, these substances may potentially migrate through clean cover and, if present at sufficiently high concentrations, may require the introduction of protective measures such as the installation of membranes in solums of buildings etc. to prevent unacceptable exposure to receptors via vapour migration and inhalation. The generation of dust during site works may also expose site operatives or the occupiers of adjacent properties to health risks and should be managed by the provision of appropriate PPE and adoption of appropriate site practices as described in CIRIA document 132 "A guide for safe working on contaminated sites".

#### Stage 3 Assessment of Risk to Other Receptors

The ecological risk assessment is carried out with respect to both on-site and off-site ecologically sensitive receptors. A review of information can indicate whether any nearby ecologically sensitive areas are likely to be impacted by on-site derived contamination; a comparison of contaminant levels found in the on-site ecologically sensitive areas can also be made with the UK Environmental Quality Standards for the protection of wildlife.

Contaminants which are at concentrations in excess of the Stage 2 screening criteria are determined to present a risk to the water environment and these contaminants therefore require assessment at a Stage 3 level. The purpose is to ascertain if the concentrations create a risk. It is important to consider factors such as the background groundwater quality, the sporadic nature of the perched groundwater and the separation of the site from the regional groundwater by an aquiclude.

The most significant receptor in the water environment assessment is considered to be the local shallow and deep groundwater. In addition there is the potential for contaminants detected on-site to detrimentally affect off-site waters. In addition deep (bedrock) groundwater resources may be important in some areas, or where groundwater may be abstracted for use. The significance of the risk to these receptors is assessed by considering, using groundwater models, the potential effects contaminants may have to groundwater and surface water receptors.

Stage 3 Evaluation of Risks to Groundwater and Surface Waters

Each receptor is considered in turn at the initial CSM stage, and investigations scoped to examine these linkages where necessary.

At Stage 2 recorded soil leachate, groundwater and surface water contaminant results are compared with GACs selected as described above, dependant on the receptor being considered (e.g. UKDWS would be used where a water abstraction was the receptor). Where exceedences of GACs occur a Stage 3 assessment is undertaken.

In the Stage 3 Risk Assessment - Water Environment a re-examination of the CSM is undertaken with respect to water environment receptors on the basis of site investigation data. Where a potential linkage remains, a back calculation is undertaken for the recorded soil leachate and/or groundwater concentration exceedences in accordance with the guidance in document WAT-PS-10-01 using the EA's Remedial Targets Methodology (RTM) and the associated Remedial Targets Worksheet hydrogeological modelling tool. After applying a dilution factor and where appropriate, degradation, the theoretical concentration of each contaminant at an assessment point is compared against the relevant assessment limit at that assessment point.

The assessment limit may be a UK Drinking Water Standard (UKDWS), Resource Protection Value (RPV) or EQS depending on the nature of the receptor which is being considered to be potentially at risk. The assessment point is the point at which assessment limit must be met. For the purposes of risk assessment the assessment point is selected to be the nearest surface water course for surface water receptors, the site boundary (or 50m downgradient of the site boundary or 250m in a sewered urban environment) for the future groundwater resource receptors or in the raw water prior to any treatment this might receive for current abstractions. It should be noted that in contrast the SEPA guidance defines a compliance point as a "real" sampling point to demonstrate that inputs are acceptable. A compliance point may be the same location as the assessment point or between the source and receptor.

In addition, where required the Remedial Targets Worksheet can be used to calculate soil remedial targets which can be used to determine whether soil contaminant levels on site require remedial actions to prevent impact to water environment receptors.

For the above calculations it is assumed that leachate is theoretically produced by water infiltration from rainfall into site groundwater which can then migrate off site. In this case the leachate migrates through permeable strata until it hits a theoretical deeper groundwater. The remedial target which is calculated represents the maximum concentration of that particular contaminant which can be allowed at the assessment point or at its location on the site in the case of soil remedial targets. If concentrations are recorded above remedial targets then theoretically by the time impacted groundwater has migrated to the assessment point it will be above the relevant assessment limit for that contaminant and remedial measures would be necessary.

Other analytical, numerical and probabilistic groundwater models are available to aid in the quantitative assessment of contaminated waters, the suitability of each which can be determined upon completion of site assessment and project requirements.

#### **RISK-BASED CONCLUSIONS**

The comparison of the estimated risks with the appropriate criteria indicates whether:-

- 1) the site presents an insignificant risk based on the analysis; or
- 2) there is a potential risk to health or the environment.

Where a risk has been identified remedial strategies can then be developed in order to break any source-pathway-receptor linkage. Strategies may include; source removal, breaking the pathway from the source to the receptor or choosing developments in which sensitive receptors are not included in areas where the risk exists.

As described above a number of remedial strategies can be adopted for a site and JPB selects the most appropriate strategy for remediation on a site specific basis. One commonly adopted practice is to break the pollutant linkages by the introduction of clean capping materials. JPB has adopted, where appropriate, the BRE/DTI/NHBC/AGS document as a decision making tool to aid the design of remedial actions.

Whilst the authors of the document acknowledge that the methodology is not sufficiently advanced to provide a basis of regulatory policy, in the absence of other authoritative guidance this document provides a research based approach to designing cover systems rather than the alternative qualitative use of professional judgement. It is, however, emphasised this document is used by JPB in the context of professional judgement and experience and a knowledge of site conditions.

As at the time of investigations the concentrations of contaminants present in material to be imported for capping may not be known, a conservative approach in which the imported material is assumed to have a contaminant concentration of 75% of the target guideline value is adopted. The spreadsheet which accompanies the document contains a viability check graph which indicates whether the capping layer calculated is acceptable or whether further consideration is required as to the effectiveness of the cover system proposed. JPB's procedure is to ensure that the effectiveness of the cover system is adequate for the site conditions encountered. Where these are exceeded more stringent remedial actions are recommended. JPB considers that this methodology provides a consistent, scientifically based rationale for designing cover systems in the vast majority of sites we encounter. Where more extreme conditions are encountered, or where there are specific site requirements, these issues will be considered on a site specific basis in order to be protective of receptors at the proposed development.

#### Remediation Strategy

Before any works can be carried out on site a Remediation Strategy must be prepared in accordance with the "Model Procedures for the Management of Land Contamination" (CLR11) and the draft document "Verification of Remediation of Land Contamination".

#### **Ground Gas Assessment Methodology**

#### Introduction

The assessment of ground gas as a potential constraint to development has been the subject of a great deal of research and published guidance. Broadly speaking ground gas can be a concern for several reasons; flammable gases may cause an explosion, build up of gases within poorly ventilated areas may lead to asphyxia or toxic gases may cause harm to those exposed to them. In general we consider principally methane and carbon dioxide levels, however the presence of other gases such as carbon monoxide, hydrogen sulphide, petroleum vapours etc may also be considered where appropriate. Some physical properties of ground gases are tabulated below.

Gas	Explosive Range	Density of 20°C	Toxicity % by volume in air*
Methane	5-15% by vol	0.72 kg/m <sup>3</sup>	30 (low)
Carbon dioxide	N/A	1.98kg/m <sup>3</sup>	0.5 (high)
Carbon monoxide	12.5-74.2% by vol	1.25kg/m <sup>3</sup>	0.02 (high)
Hydrogen sulphide	4.2-46% by vol	1.54kg/m <sup>3</sup>	0.001 (high)

<sup>\*</sup> short term exposure limits

These ground gases may originate from many sources including; mine workings, organic sediments, landfilling, biodegradable materials in made ground on brownfield sites, petroleum hydrocarbons or other site specific sources. The gas concentrations measured are the result of volatile emissions and the microbial degradation of organic materials. The processes by which materials degrade to form ground gases are discussed more fully in Waste Management Paper 27 (2<sup>nd</sup> Ed, 1999) and Waste Management Paper 26A (1993).

JPB's overall methodology for ground gas assessments is summarised in the attached flow chart. In order to assess the degree of risk to receptors we must first develop a conceptual site model (CSM) of the site which can identify the various sources and receptors and any potential pathways by which they may be linked. This process can be undertaken as part of the development of a CSM for the site for contaminants other than gases. If a potential pollutant linkage is identified for ground gas, site investigations to confirm the nature and extent of ground gases will be required. Guidance on how these site investigations should be undertaken is given in B5930 (1999) - Code of Practice for Site Investigations, BS10175:2001 - Investigation of Potentially Contaminated Sites, CIRIA Reports 103 (Vol II) and 150 (Methane Investigation Strategies), CIRIA C665 (2007) and BS8485: 2007 and other published guidance.

Investigation methodologies which have been used to measure gas concentrations include spike probe surveys, sinking of boreholes with monitoring standpipes installed and flux boxes. Spike probe surveys are considered to be unreliable for the following reasons: limited depth, spikes into an aerobic layer in an open hole underestimate methane levels and spike probes may not intercept the gas source.

In preference JPB therefore generally commissions the sinking of boreholes with standpipes to characterise the gas regimes at sites. Where access is restricted, a window sampler is used to install standpipes. The number and position of bores and well response zones are carefully chosen in order to maximise the information to be obtained to fully characterise the site. Table 4.2 in CIRIA C665, reproduced below, gives some guidance on the spacing of wells, which should be interpreted in conjunction with the associated text of that paper.

Gas Hazard	Typical examples	Sensitivity of end	Initial nominal spacing of gas
		use	monitoring wells <sup>1,2</sup>
High	Domestic landfill sites	High <sup>3</sup>	Very close (<25m)
		Moderate	Close (25-50m)
		Low	Close (25-50m)
Moderate	Older domestic landfills disused	High	Close/very close (<25m -50m)
	shallow mine workings <sup>4</sup>	Moderate	Close (25-50m)
		Low	Close/wide (25-75m)
Low	Made ground with limited degradable	High	Close (25-50m)
	material, organic clays of limited	Moderate	Wide (50-75m)
	thickness	Low	Wide/very wide (50->75m)

- <sup>1</sup> The initial spacing may need to be reduced if anomalous results indicate this is necessary to give a robust indication of the gas regime below a site. To prove the absence of gas, closer spacings may be required.
- The spacing assumes relatively uniform ground conditions and the gas source present below a site. The spacing will need to be reduced if ground conditions are varied or if the investigation is trying to assess migration patterns from off site.
- Placing high-sensitivity end use on a high gas hazard site is not normally acceptable unless the source is removed or treated to reduce gassing potential.
- Petrol stations and other sources of vapours are most likely to be classified as gas hazard "Moderate" however site specific assessment would be required.

Three bores with standpipes and four sets of readings should be considered an absolute minimum for even the smallest of sites

Flux boxes can be used to measure surface gas emission rates but do not take into account a deeper source of gas generation. Flux boxes can be used to confirm that a capping layer above a source and the surface has been effective. It should be noted that methane levels at the surface may underestimate ground gas levels as aerobic conditions at the near surface will deplete methane concentrations.

Guidance on the measurement of gas levels at bores is given in the above documents, however in general a peak gas reading is taken followed by readings at 30 second intervals until a steady state is reached. This allows the assessor to determine how quickly the ground gas is replenished. Flow rate is generally measured first followed by methane/carbon dioxide levels. In addition atmospheric pressure, weather, date and any other relevant information is recorded.

Flow rates can be positive or negative, they are generally negative where ambient atmospheric pressure is high or where falling groundwater levels reduce pressures in bores. Flow rates between -0.4 and 0.4 L/h indicate that there is probably no overall flow. The length of the monitoring period and frequency of monitoring will vary from site to site depending on the sensitivity of development, geology of the site, the level of risk and other factors. Typical minimum periods and monitoring frequencies are given in Table 5.5 of CIRIA C665. Generally JPB performs a minimum of four visits over the course of a 4-6 week period.

The degree of monitoring required must enable the assessor to measure or predict the worst case gas regime.

#### Risk Assessment

Having obtained factual data from the investigation the ground gas regime can be assessed in a tiered approach. In the past guidance such as Waste Management Paper 27 recommended a highly conservative precautionary principle, i.e. no development within 250m of a landfill site. This approach was seen as anti-development and does not take into account the site conditions, whether a risk exists at the site for the development proposed, the level of risk and whether if can be mitigated by design. More recent approaches characterise the site and the risk and base recommendations on this assessment. Various reports and standards have recently been published to update the guidance on ground gas assessment and this JPB methodology uses the philosophy outlined in these. These include CIRIA C665 "Assessing risks posed by hazardous ground gases to buildings" (2007), NHBC Report No. 10627-R01(04) "Guidance on evaluation of development proposals on sites where methane and carbon dioxide are present" (2007) and British Standard BS8485 (2007) "Code of practice for the characterisation and remediation from ground gas in affected developments".

### Tier 1 assessment

Following the completion of investigations the assessor reviews the CSM in the light of site investigation data and identifies any intact pollutant linkages. If intact pollutant linkages exist a Tier 1 risk assessment is performed using generic screening criteria to determine whether a risk exists. JPB uses the following screening levels: **Methane <1%** by volume in boreholes and Carbon dioxide <5% by volume in boreholes.

These values are derived from Waste Management Paper 27, 1% methane by volume represents 20% of methane's lower explosive limit of 5% by volume, 5% carbon dioxide relates to the known health effects of exposure to this gas. Both screening concentrations are detailed in the Building Regulations Approved Document C (2004) and BRE Report "Construction of New Buildings as Gas Contaminated Land" (BR 212).

A limit to gas flow rates for the above trigger values is inferred by the table given below where the limiting borehole gas volume flows for  $CH_4$  and  $CO_2$  are <0.07L/hr for characteristic situation 1. These are equivalent to a limiting borehole flow rate of 7L/h for  $CH_4$  at 1% by volume and 1.4L/h for  $CO_2$  at 5% by volume. The above Tier 1 trigger values are only valid, therefore, if these volume flows are not exceeded. Where these volume flows are exceeded a Tier 2 assessment should be undertaken.

It is understood that new guidelines on screening levels for hydrogen sulphide and other trace gases will be issued in CIRIA RP711. Other information on VOCs is available in EA Technical Guidance on Management of Landfill Gas (2004) and in the vapour models used in the CLEA model for contamination land assessments.

If these screening concentrations are not exceeded then no significant risk exists and no further action is required. Where screening concentrations are exceeded a Tier 2 assessment is performed.

#### Tier 2 assessment

Where Tier 1 generic screening concentrations are exceeded a Tier 2 assessment is performed using the Wilson and Card (1999) approach as outlined in CIRIA C665. Each site is classified into a "characteristic situation" based on the maximum methane and carbon dioxide concentrations measured. These measurements combined with the maximum borehole flow rate are used to calculate the gas screening value.

Gas screening value (L/hr) = gas concentration (% by volume) x borehole flow rate (L/hr).

(N.B. gas screening value is also known as "site characteristic hazardous gas flow rate (Qhos) in BS8485)

For example for a borehole flow rate of 1.5 L/h and a methane concentration of 20% the gas screening value =  $1.5 \times 20/100 = 0.3 \text{ L/h}$ .

Gas screening value rates for methane and carbon dioxide can be compared with Table 8.5 of CIRIA C665 "Assessing risks posed by hazardous ground gases to buildings" (2007) or Tables 14.1 of NHBC Report No. 10627-R01(04) "Guidance on evaluation of development proposals on sites where methane and carbon dioxide are present" (2007), reproduced below, to determine a characteristic situation for the site.

Table 8.5 Modified Wilson & Card Classification (CIRIA Report C665)

NB Use for most scenarios other than low rise housing with a ventilated underfloor void (min 150mm)

Characteristic Situation (CIRIA R149)	Comparable classification in DETR et al (1999)	Risk classification	Gas Screening Value (GSV) CH <sub>4</sub> or CO <sub>2</sub> (L/hr) <sup>1</sup>	Additional Limiting Factors	Typical Source of generation.
1	А	Very low risk	<0.07	Typically methane <1% by volume and/or carbon dioxide < 5%. Otherwise consider increase to Situation 2.	Natural soils with low organic content. "Typical" made ground
2	В	Low risk	<0.7	Borehole air flow rate not to exceed 70L/hr. Otherwise increase to characteristic situation 3	Natural soil, high peat/organic content. "Typical" made ground
3	С	Moderate risk	<3.5		Old landfill, inert waste, mineworking flooded
4	D	Moderate to high risk	<15	Quantitative risk assessment required to evaluate scope of protection measures	Mineworking – susceptible to flooding, completed landfill, inert waste (WMP 26B criteria)
5	Е	High risk	<70		Mineworkings unflooded inactive
6	F	Very high risk	>70		Recent landfill site

Table 14.1 Gas Risk Assessment (Traffic Lights) NHBC Report No. 10627-R01(04)

NB To be used for low rise housing with a ventilated underfloor void (min 150mm)

vpical max conc. <sup>5</sup> % by vol)	Gas screening value <sup>2,4,6</sup> (L/hr)	Typical max conc. <sup>5</sup> (% by vol)	Gas screening value <sup>2,3,4,5</sup> (L/hr)
1	0.13	5	0.78
5	0.63	10	1.60
20	1.60	30	3.10

#### Radon

Radon is a naturally occurring radioactive gas that is formed from the decay of uranium and radium present in some types of rocks. It can migrate through cracks and fissures into the soil and by this route into buildings.

Radon can accumulate inside structures over the long term posing a risk to health. Long term exposure increases the risk of developing lung cancer, in a building with high levels of radon, long-term exposure can increase the risk to the point where preventative action is necessary.

BRE 211 provides guidance on how the risks posed by radon should be assessed. JPB's methodology for assessing risks posed by radon follows that guidance and this methodology is outlined below.

The location of the site is pinpointed on maps within the "Indicative Atlas of Radon in England and Wales", published in July 2007. This document was the result of a joint project between The Health Protection Agency (HPA) and the British Geological Society who prepared detailed maps of radon potential by testing radon levels in houses. Where tests on existing houses show that 1% of the houses in a particular area are likely to have a radon concentration above 200 Bq/m³ (the action level) the area is designated as a 'radon affected area'.

Where the site is indicated to be within a radon affected area, a more detailed risk report giving the estimated radon potential for the specific site is obtained through the HPA radon website www.UKradon.org. If this report indicates that the site is located on ground designated as a 'radon affected area', or on ground where radon is known to exist, protective measures are recommended. Radon protective measures are recommended in accordance with the guidance contained in BRE publication BR 211 – 'Radon: guidance on protective measures for new buildings'.

It should be noted that this approach has been adopted as monitoring radon concentrations in the ground prior to construction is not considered to be a valid methodology for assessing risks posed by radon in buildings. This is because it is difficult to equate the concentrations of radon measured in boreholes with levels inside houses, as many factors can influence the actual indoor air radon concentration experienced, including; radon generation rates, geology, construction details, ventilation rates, seasonal factors, occupant behaviour etc. Similarly, for newly constructed buildings it is impractical to determine indoor air radon concentrations over the recommended three month monitoring period and the results measured in unoccupied properties would not, in any case, be a valid assessment of conditions in occupied houses.